

### QUEANBEYAN SEWAGE TREATMENT PLANT UPGRADE PROJECT

# Masterplan for Sewage Treatment Plant Upgrade









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### **Queanbeyan Sewage Treatment Plant Upgrade Project**

#### Masterplan

Owner	Queanbeyan Palerang Regional Council
Prepared by	Dr Therese Flapper et al, GHD Pty Ltd; Peter Cox, QPRC
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## **Executive Summary**

The Queanbeyan Sewage Treatment Plant (STP), constructed in the mid-1930s, treats effluent from the Queanbeyan Local Government Area (LGA), prior to discharge into the Molonglo River. While maintenance works are regularly undertaken on the STP, the plant is no longer fit-for-purpose. A significant works program is required to address issues including structural failure, equipment obsolescence, maintenance issues and work health and safety issues, as well as refining the process train.

This upgrade project has been instigated as a result of the following drivers for the site:

- Capacity required for current and future population growth
- Much of the existing infrastructure at or approaching end of asset life
- Operability and reliability issues of the STP
- Providing a level of service that conforms to industry best practice for the protection of public health and the environment
- A facility that meets regulator/stakeholder concerns/requirements
- Optimisation of STP design to achieve Infrastructure Sustainability Council of Australia (ISCA) rating of 'Excellent' or 'Leading'.

This Masterplan sets out the design basis for proceeding with the upgrade of the STP, as summarised below.

In conclusion, a 60,000 EP STP is recommended to be constructed on the current site. For future upgrades and additions to the treatment facility, further investigation will be required in accordance with the Road Map (refer Figure 1-1).

Masterplan Element	Design Basis Outcome
Best for region Solution	Queanbeyan's location on the border of NSW and the ACT puts it in a unique position. The STP is located in the ACT on leased land and ACT Environment and Planning Directorate (EPD) (which includes the Environment Protection and Water Regulation Division), ACT Health and the National Capital Authority (NCA) regulate various aspects of the STP operations. Potential regional opportunities for wastewater management are subject to ongoing
	discussion with the ACT Government and Icon Water.
Future Growth	Growth is expected to occur in the middle portion of the LGA within the 10 to 25-year horizon. The southern third of the LGA is then expected to grow during the 25 to 50-year horizon.
	Provision for the first stage of the Queanbeyan STP Upgrade should be for an EP of 60,000. This provides for the 10 to 15-year growth projection. It should be noted that the projections within this Masterplan do not make allowance for any ACT contribution to sewage flows, though depending on timing of actual increases, some flow may be able to be accommodated.
	The EP calculator was based on average water data for Queanbeyan LGA averaged over 2009-14.





Masterplan Element	Design Basis Outcome
Existing Sewerage Infrastructure	The existing Queanbeyan STP condition currently presents a risk to QPRC with numerous suggestions for both immediate and short-term improvement. Beyond operability and WHS issues, there will be a stronger focus on water quality and environmental discharges. Tighter discharge criteria are likely to be imposed in the future when licence conditions are re-negotiated.
Future Sewerage Infrastructure	<ul> <li>The South Jerrabomberra sewer trunk will need to be upgraded to meet future capacity: <ul> <li>Consider augmentation of the Jerrabomberra Trunk Sewer between manholes W8 and the inlet channel of the STP</li> <li>Any further augmentation should be delayed until a final service strategy is decided for future development to the south of Queanbeyan</li> <li>A survey and sewer gauging program should be implemented for the whole length of the trunk sewer (manhole W78 to the STP inlet channel) to enable a more detailed analysis of the sewer</li> </ul> </li> <li>Continue discussions with Icon Water around cross-border arrangements and a regional approach to sewage management.</li> <li>A septic tank receival station should be included in the new plant.</li> </ul>
Environmental Constraints	<ul> <li>The following should be considered when determining the location for future STP(s):</li> <li>Avoid heritage listed sites, scenic protection areas, and quarry buffer zone</li> <li>Construction within the ANEF affected areas could be considered if appropriate as aircraft noise is unlikely to be an impact on STP operations</li> <li>Avoid infrastructure within the Q100 flood level without proper flood protection or mitigation measures in place</li> <li>Avoid bushfire prone areas or provide adequate protections, appropriate to STP operations</li> <li>Consider and incorporate mitigation of environmental issues on existing site as part of concept design.</li> </ul>





Masterplan Element	Design Basis Outcome				
Water Quality	Adopt the following effluent discharge criteria and 100% river discharge as the basis of design outcome.				
	Parameter	Units	Performance	Statistic	Proposed Licence Limit (100%ile)
	Total Nitrogen	mg/L	10 5	90%ile 50%ile	10
	Total Phosphorus	mg/L	0.15 0.1	90%ile 50%ile	0.2
	Faecal coliforms	cfu/100mL	30 200	Median 90%ile	60
	BOD	mg/L	10 5	90%ile 50%ile	10
	Suspended Solids	mg/L	10 5	90%ile 50%ile	10
Sustainability	<ul> <li>Set sustainability targets with the goal of obtaining IS design and as-built ratings of Excellent with a score in the range of 65 – 75% or better.</li> <li>Undertake a recycled water study to determine the viability of reuse in the future which addresses impacts on:</li> <li>1. Discharge to the Molonglo River</li> <li>2. Molonglo River yield and downstream environmental flows</li> <li>3. Aquatic species along the Molonglo River.</li> </ul>				
Solids Management	<ul> <li>The solid management solution comparison showed that the most beneficial options were:</li> <li>Reuse for land reclamation</li> <li>Production of fertiliser for animal crops</li> <li>Production of fertiliser for human crops</li> <li>Use for horticulture and landscaping.</li> <li>The concept design phase should develop and consider these options further, however if other feasible options become apparent then these may also be considered.</li> <li>A regional strategy for solids management is required but is outside the scope of this project.</li> </ul>				





Masterplan Element	Design Basis Outcome		
Treatment	Treatment Step	Preliminary Option	
Technologies	Preliminary	Inlet works screenings and grit removal to be determined by choice of the secondary treatment process.	
	Primary	Equalisation tanks or Primary settling and possible use of mechanical belt sieve.	
	Secondary (one of)	<ul><li>BNR Bio-Reactor plus one of</li><li>Membrane Bioreactor (MBR)</li><li>Conventional Activated Sludge (CAS), e.g.</li></ul>	
		<ul> <li>Sequencing Batch Reactor/ Intermittently Decanted Aerated Lagoons (SBR/IDAL)</li> </ul>	
		<ul> <li>Pasveer/Oxidation ditch</li> </ul>	
	Tertiary (one of)	<ul><li>Tertiary Filtration</li><li>Refurbishing secondary clarifiers</li></ul>	
	Disinfection	UV Chlorine (if required for regulatory purposes)	
	Solids	Grit and Screenings - Landfill	
	Biosolids (one of or a combination of)	<ul><li>Land reclamation</li><li>Animal crop production</li></ul>	
	,	Landscaping – Composting	
		Other options may be considered if they can be shown to be feasible through a regional approach.	
Upgrade approach	A Multi Criteria Assess taking into account wh proofing and commun	sment found that a "Build New" upgrade approach was preferred nole of life cost, constructability, operability, sustainability, future ity acceptance and affordability.	
	All options including b NPV around \$100 M. modelling showed a m	uild new, refurbishment and reuse options provided a whole of life The total project cost estimate prepared by QPRC using @risk nean estimated project value of \$108 M.	
	The assessment of pla investment saving cor preliminary and based within the sensitivity o	ausible refurbished and reused assets showed no significant capital npared to the build new option cost estimates. All estimates are I on a range of caveats. There is no discernible significant difference f the cost analysis at a Masterplan level.	
	The selection of treatmoutcome.	nent technology (BNR – CAS v BNR – MBR) was not significant to the	





Masterplan Element	Design Basis Outcome
Approvals	ACT Approvals
	Under Schedule 4 of the ACT <i>Planning and Development Act 2007</i> (P&D Act) the proposed upgrade to the STP would require an environment impact statement (EIS).
	A Development Application (DA) would also be required and would likely be assessed under the Impact Track. The completed EIS is required to be submitted with the Development Application submitted under the Impact Track. This applies to the whole site zoned TSZ2: Services and NUZ4: River Corridor (small areas bordering the Molonglo River).
	NSW Approvals
	NSW approvals will be required for any works within NSW (such as the sewerage collection system). The NSW legislation would similarly require Development Approval and environmental consideration (such as contaminated lands and endangered species). It is possible that the approving authority for this work could be QPRC. Further detail of the scope of any works in NSW would be required to determine this.
	NSW Department of Primary Industries, Water Department (DPI Water) is required to approve the STP upgrade under Section 60 of the <i>Local Government Act (1993)</i> .
	Federal Approvals
	Any works approval sought needs to consider the <i>Environmental Protection and Biodiversity Conservation Act 1999</i> .
	General Comments
	In 2015 the interim ACT and Region Catchment Management Coordination Group was formed by the ACT Environment Minister. This group includes EPD, and other ACT Government Stakeholders. The function of this committee is to implement an integrated catchment management approach in the ACT and Region, including improving water quality in Lake Burley Griffin.
	Continued engagement with EPD, ACT Government Stakeholders, NSW EPA and the NCA will be required regarding Lake water quality improvement through an agreed approach and throughout the preparation of the EIS. A framework for a joint approach is agreed.
	Local Councils are required to produce an Integrated Water Cycle Management (IWCM) plan outlined by NSW DPI Water.



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#### Figure 1-1 Road Map of options





# **Executive Sign-Off**

Position	Name	Signature
QPRC Director of Projects and	Phil Hansen	Al
Assets		
QPRC Acting General Manager	Peter Tegart	a
QPRC Administrator	Tim Overall	





### **Abbreviations**

Abbreviation	Description
ACT	Australian Capital Territory
ADWF	Average dry weather flow
ANEF	Australian noise exposure forecast
AS	Australian Standard
BNR	Biological nutrient removal
BOD	Biological oxygen demand
Сарех	Capital expenditure
Cfu/100 mL	Colony forming units per 100 millilitres
CSS	Canberra Sewage Strategy
DA	Development application
DN	Nominal diameter
DPI Water	Department of Primary Industries Water Department
EIA	Environmental impact assessment
EIS	Environmental impact statement
EP	Equivalent population
EPA	Environmental Protection Authority
EPBC	Environmental Protection and Biodiversity Conservation Act 1999
EPD	ACT Government Environmental and Planning Directorate
EPL	Environmental protection licence
EPP	Contaminated Sites Environmental Protection Policy 2009
g/EP/d	Grams per equivalent population per day
ha	Hectare
HWA	Hunter Water Australia
IDAL	Intermittently decanted aerated lagoon
IFAS	Integrated fixed film activated sludge
IS	Infrastructure sustainability





Abbreviation	Description
ISCA	Infrastructure Sustainability Council of Australia
IWC	Integrated water cycle
IWCM	Integrated water cycle management
kg/d	Kilograms per day
km	Kilometre
LBG	Lake Burley Griffin
L/EP/d	Litres per equivalent population per day
LGA	Local Government Area
LMWQCC	Lower Molonglo Water Quality Control Centre
L/s	Litres per second
m	Metre
mm	Millimetre
m <sup>3</sup> /s	Cubic metres per second
MBBR	Moving bed bioreactor
MBR	Membrane bioreactor
mg/L	Milligrams per litre
ML/d	Megalitres per day
MLRMC	Mugga Lane Resource Management Centre
NCA	National Capital Authority
nm	Nanometre
NOW	Formally - New South Wales Office of Water
	Presently - the Department of Primary Industries Water Department (DPI Water)
NSW	New South Wales
NZS	New Zealand Standard
OPEX	Operational expenditure
P&D Act	Planning and Development Act 2007
PDWF	Peak dry weather flow





Abbreviation	Description
PMF	Project management framework
PRA	Preliminary risk assessment
PWWF	Peak wet weather flow
QPRC	Queanbeyan Palerang Regional Council
Qf	Pipe capacity
Q100	100 year average recurrence interval flood
RAS	Return activated sludge
SBR	Sequencing batch reactor
STP	Sewage treatment plant
t/y	Tonne per year
TN	Total nitrogen
ТР	Total phosphorus
TSS	Total suspended solids
VENM	Virgin excavated native material
Vsc	Self-cleaning velocity in sewer
WHS	Work health and safety
WQOA	Water quality objective assessment
WRP	Water recycling plant
μm	Micrometre





## **Table of Contents**

1	Introduction		1
	1.1	Overview	1
	1.2	Project drivers	2
	1.3	Scope of masterplan	2
2	STP	upgrade regional context	3
	2.1	Geography	3
	2.2	Climate	3
	2.3	Land development	3
	2.4	Regional sewerage infrastructure	7
	2.5	'Best for region' sewage treatment solution	7
3	Futu	re growth	9
	3.1	Population projection	9
	3.2	Concluding observations	10
4	Exis	ting sewerage infrastructure	12
	4.1	Queanbeyan sewage collection network	12
	4.2	Sewage quality	16
	4.3	Queanbeyan Sewage Treatment Plant (STP)	16
	4.4	Concluding observations	21
5	Futu	re sewerage infrastructure	28
	5.1	South Jerrabomberra	28
	5.2	Googong Township	33
	5.3	Concluding observations	33
6	Envi	ronmental constraints	35
	6.1	Heritage reserve	35
	6.2	Scenic protection	36





	6.3	Quarry buffer	37
	6.4	Australian Noise Exposure Forecast (ANEF)	38
	6.5	Floodplains	39
	6.6	Bushfire prone areas	41
	6.7	Review of current site	42
	6.8	Concluding observations	44
7	Wate	r quality objectives assessment	45
	7.1	Scope	45
	7.2	Water quality data review outcomes	47
	7.3	Water quality modelling approach	48
	7.4	Water quality model findings	48
	7.5	Setting effluent quality objectives	50
	7.6	ACT EPA licence requirements	50
	7.7	STP bypass event modelling	50
	7.8	Concluding observations	51
8	Susta	ainability	52
	8.1	General	52
	8.2	ISCA and the IS rating tool	52
	8.3	Reuse of Effluent	53
	8.4	Concluding Observations	53
9	Treat	ment technology approaches	54
	9.1	Preliminary	54
	9.2	Primary	54
	9.3	Secondary	54
	9.4	Tertiary	56
	9.5	Disinfection	56
	9.6	Sludge handling	57





	9.7	Ancillary processes	58
10	Solid	ls management	59
	10.1	Introduction	59
	10.2	Local regional solution	59
	10.3	Agricultural land application	60
	10.4	Non-agricultural land application	61
	10.5	Energy recovery – Renewable energy resources	62
	10.6	Other uses	62
	10.7	Comparison	62
	10.8	Concluding observations	63
11	Optic	ons Road Map	64
	11.1	STP location and staging	64
12	Upgr	ade Options	75
	12.1	Introduction and Background	75
	12.2	Approach and Method	75
	12.3	Existing STP Condition	75
	12.4	Upgrade Options	76
	12.5	Cost Estimates	77
	12.6	Multi-Criteria Analysis	77
	12.7	Concluding Remarks	79
13	Risk	Based Cost Estimate	80
	13.1	Approach	80
	13.2	Concluding observations	81
14	Stake	eholders	82
	14.1	Engagement	82
	14.2	Community consultation	82
15	Interi	im and transition infrastructure requirements	83





	15.1	Inlet screens	83
	15.2	Final clarifiers	83
	15.3	Sludge Lagoons	84
	15.4	Timing	84
16	6 Approvals		
	16.1	Planning	85
	16.2	Environmental Approvals	86
	16.3	Infrastructure approvals	88
	16.4	IWCM	91
17	Basis	of design outcome	92
18	References		

### **Table index**

Table 3-1	EP projection Inclusive / Exclusive of Googong as per EP Calculator projections	10
Table 4-1	Length of Queanbeyan sewers renewed by age	13
Table 4-2	Short and long term options for treatments	23
Table 5-1	Sewer Capacity Criteria	29
Table 5-2	Sewage Loads on the Jerrabomberra trunk sewer	30
Table 5-3	Outcomes of analysis	31
Table 5-4	Summary of risks	33
Table 6-1	Current site environmental aspects and potential mitigation	42
Table 7-1	Scenarios used for WQOA	45
Table 7-2	WQOA outcomes for performance of STP and proposed licence limits	51
Table 10-1	Solids management solution comparison (criteria scores shown are out of 10)	63
Table 12-2	QSTP Upgrade Options	76
Table 12-3	MCA Criteria Weighting	78
Table 12-4	MCA Results and Rank	78
Table 17-1	Basis of design	92
<b>—</b>	the states	

### **Figure index**

Figure 1-1 Road Map of options			
Figure 2-1	Future development areas in Queanbeyan LGA	5	
Figure 2-2	ACT Eastern broadacre development investigation areas	6	
Figure 3-1	Population projections for the Queanbeyan LGA	10	
Figure 4-1	Age of the QPRC LGA sewer network	14	
Queanbeyan Sev	vage Treatment Plant Masterplan		
Last saved; REV	5 / 22 September 2016		





Figure 4-2	Distribution of relined sewer mains in the QPRC LGA	15
Figure 4-3	Queanbeyan STP process flow and discharge to Molonglo River	17
Figure 5-1	Proposed future land uses of South Jerrabomberra	28
Figure 5-2 Jerrabomberra	Expected condition of the Jerrabomberra trunk sewer after 10 years (Image from Sou Structure Plan 2013)	th 32
Figure 6-1	Heritage reserve areas in the QPRC LGA	35
Figure 6-2	Scenic protection areas in the QPRC LGA	36
Figure 6-3	Quarry buffer area in the QPRC LGA	37
Figure 6-4	ANEF for airport noise levels in the QPRC LGA	38
Figure 6-5	Floodplain areas in the QPRC LGA	39
Figure 6-6	Contour of Q100 flood line in relation to Queanbeyan STP infrastructure	40
Figure 6-7	Areas in the QPRC LGA with significant bushfire risk	41
Figure 7-1	WQOA locations	46
Figure 7-2	Total phosphorus concentration of STP effluent at location 4 (downstream of the STP	) 49
Figure 7-3	Total nitrogen concentration of STP effluent at location 4 (downstream of the STP)	49
Figure 11-1	Road map for possible options	66
Figure 11-2	Proposed first development	67
Figure 11-3	Option 1 between 10 and 25 years	68
Figure 11-4	Option 2 between 10 and 25 years	69
Figure 11-5	Option 1A between 25 and 50 years	70
Figure 11-6	Option 1B between 25 and 50 years	71
Figure 11-7	Option 2A between 25 and 50 years	72
Figure 11-8	Option 2B between 25 and 50 years	73
Figure 11-9	Option 2C between 25 and 50 years	74
Figure 12-1	Reuse Potential of QSTP	76
Figure 13-1	Risk based assessment of total estimated project costs	81
Figure 16-1	Five step approval process for NSW Office of Water	90

### **Appendices**

Appendix A Population Forecast and EP Calculator Appendix B Growth Concentration Appendix C Regulatory Roadmap Appendix D Water Quality Objective Assessment Appendix E Stakeholders Appendix F Solids Management Appendix G Technology Summary





### Appendix H Secondary Treatment Options Appendix I Condition Assessment Appendix J Technical Memoranda on Current Operations Appendix K Technical Memoranda TM004 – Upgrade Options





### 1 Introduction

### 1.1 Overview

The Queanbeyan Sewage Treatment Plant (STP) was constructed in the mid-1930s and treats Queanbeyan's sewage prior to discharge of effluent into the Molonglo River. While maintenance and works are regularly undertaken on the STP, the plant is no longer fit-for-purpose. A significant works program is required to address issues including structural failure, equipment obsolescence and maintenance issues, as well as refining the process train.

In early 2011, Queanbeyan Palerang Regional Council (QPRC) was faced with growing concern about the capacity and reliability of the Queanbeyan Sewage Treatment Plant (STP), and engaged Hunter Water Australia P/L (HWA) to prepare an options study to upgrade the STP. This study recommended a major upgrade to the plant including construction of new inlet works and a new membrane bioreactor (MBR) process with combined biological/chemical phosphorus removal, single sludge stream and aerobic sludge digestion. Since that time the condition of assets on site has continued to deteriorate and the population has increased resulting in the design capacity of the existing plant being exceeded. The existing STP is estimated to have a design equivalent population (EP) of 34,500 (MWH, 2008) and is currently serving about 37,000 EP.

While the STP is meeting current effluent licence conditions, the maturation lagoons are a key asset in achieving this effluent quality and there is a risk that these lagoons may fail again as occurred in 2010 due to flooding.

Some of the existing equipment is obsolete and there are issues with maintenance of the existing plant. There is the potential that the current process is unable to meet more stringent discharge criteria if imposed in the future.

It is estimated that the existing Queanbeyan STP has about 3 to 5 years' effective service life remaining before its condition or ability to meet load requirements presents a major risk to QPRC and the community. This assessment is based on the previous studies undertaken at the plant (e.g. MWH (2008) and HWA (2011) and the recent Condition Assessment undertaken as part of this Masterplan work (GHD, TM003, July 2105).

On these grounds, QPRC has proposed to undertake the upgrade of the Queanbeyan STP. The aim of the upgrade project will be to have a STP that provides a level of service that conforms to industry practice for the protection of public health and the environment.

The project consists of the planning, design and construction of sewage collection, treatment and disposal facilities to serve Queanbeyan within the Queanbeyan Palerang local government area (LGA). QPRC intends to deliver the project in six distinct phases to provide hold points that will facilitate proper buy-in by regulators and other stakeholders for the Queanbeyan Sewage Treatment Plant Upgrade. QPRC has completed Phase 1 Project Inception and Phase 2 Project Delivery Plan of the project. This document is the output from Phase 3 - Masterplan and Feasibility.





#### 1.2 Project drivers

The following drivers have instigated this upgrade project by QPRC:

- Capacity required for current and future population growth
- · Asset life of existing infrastructure, as there is little remaining useful life for some of the existing assets
- Operability and reliability of STP
- Desire for a new STP to provide a level of service that conforms to industry best practice for the protection of public health and the environment
- STP design that meets regulator/stakeholder concerns/requirements
- Optimisation of STP design to achieve Infrastructure Sustainability Council of Australia (ISCA) rating of 'Excellent' or 'Leading'.

#### 1.3 Scope of masterplan

This Masterplan establishes the framework and constraints for the upgrade project. Issues examined include existing infrastructure in Queanbeyan and the surrounding region, future growth, environmental constraints, water quality objectives and technology selection.

This Masterplan identifies the infrastructure that best meets expected growth and development of Queanbeyan. Some of the key matters addressed by the Masterplan include:

- Stakeholder consultation regarding objectives / expectations, cross border arrangements, cross border regulation, key design criteria, and service strategies and options
- Review of existing sewage collection and treatment arrangements for Queanbeyan including demands, inflows, influent quality, service level, and service costs
- Review of future growth projections for Queanbeyan LGA
- A water quality objectives analysis (WQOA) to identify treatment criteria in terms of public health and environment protection; particularly for the Molonglo River and Lake Burley Griffin
- Options for providing services to meet future needs including potential for recycled water reuse, decentralised services, energy and carbon footprint reduction
- Review of treatment technologies (including emerging trends) and their advantages and disadvantages that could be adopted for Queanbeyan to meet agreed treatment criteria
- Masterplanning options workshop to compare and rank the various treatment options, and initiate approvals processes
- Review of environmental and operational risks that could adversely affect project outcomes
- Review of approved requirements
- Review of the project and that the project is still economically sound.

The timeframe for this Masterplan is a 50-year planning horizon. This means that the constraints and issues identified and considered now will also be considered into the future.





### 2 STP upgrade regional context

#### 2.1 Geography

#### 2.1.1 Queanbeyan Palerang Local Government Area (LGA)

Queanbeyan is a regional centre in the Southern Tablelands in south-eastern New South Wales (NSW) adjacent to the Australian Capital Territory (ACT). The city's mixed economy is based on light construction, high technology, manufacturing, service, retail and agriculture. At the 2011 census, Queanbeyan had a population of 37,991. The LGA is characterised by a medium density urban centre at Queanbeyan City in the north and rural residential blocks in the south. Growth areas have been identified through the central corridor of the LGA as identified in Figure 2-1.

#### 2.2 Climate

According to the Bureau of Meteorology, Queanbeyan's climate, and the surrounding region, is characterised by hot summers (mean maximum 29 °C) and cold winters (mean minimum -0.2 °C). Mean annual precipitation is 594.8 mm. These conditions will need to be considered in the design phase of the STP Upgrade Project.

#### 2.3 Land development

According to the QPRC website:

"Queanbeyan is one of NSW's fastest growing cities with our population set to grow from 42,000 to around 70,000 in the next 20 years."

#### 2.3.1 South Jerrabomberra

A significant development area of relevance for the Queanbeyan STP upgrade project is the South Jerrabomberra Development Area. The South Jerrabomberra site is located in NSW south of Queanbeyan, near the existing suburb of Jerrabomberra, and adjacent to the Hume industrial area in the ACT. Land in the region has previously been occupied by homesteads and grazing land, and is bordered on the northwest by the Queanbeyan-Cooma Railway Line. The 417 ha South Jerrabomberra area is anticipated to eventually have approximately 4,700 homes.

A number of developments are anticipated in the area, which will be a mix of residential, commercial and industrial developments. The anticipated neighbourhood developments are (listed in order from north to south):

- Poplars primarily industrial/commercial development
- Environa and North Tralee primarily industrial development
- South Tralee primarily residential development
- Forrest, Morrison and Walsh (land to the south of South Tralee) residential areas.

A range of community and recreational facilities have been proposed including an aquatic centre, a regional sporting complex (Poplars), open space and sporting fields, a private secondary college and a primary school. Two local centres have been identified for retail and commercial purposes within Poplars and South Tralee. A 250 m wide open area is planned as a buffer between South Jerrabomberra and the adjacent Hume light industrial area.

These developments are likely to progress in a series of stages over a period of 25 years. Initial construction will begin with South Tralee, including works on access, sewer, water, electricity and gas. About 1,300 homes are eventually expected to be contained in this first neighbourhood of approximately 180 ha area.





#### 2.3.2 Googong Township

Googong Township is located near Googong Dam off Old Cooma Road, 5 km south of the Queanbeyan Central Business District. The region is characterised by gently undulating slopes and plains and used originally for grazing land. The 780 ha Googong development is planned to have around 5,550 homes for approximately 16,000 people, as well as schools, parks, shops and businesses.

Infrastructure development for the Googong Township includes:

- Upgrade of access roads between Queanbeyan and Googong
- Installation of a sewage treatment plant (water recycling plant) (WRP) to deliver recycled water to homes for non-potable use including toilet flushing, fire-fighting and irrigation for gardens and public parks and spaces
- The WRP includes potable and recycled water reticulation networks, pump stations, reservoirs and sewage collection network
- Construction of a multi-purpose community centre and library, indoor sports and aquatics centre, two neighbourhood community centres and a community clubhouse
- A variety of parks, playgrounds and sporting field facilities, as well as a network of walking and bike paths
- New waterways and ponds
- Provision of gas services and telecommunication coverage.

The Township is comprised of five neighbourhoods, with North Googong being the first to be developed. Each neighbourhood has a central hub ranging in size from several shops to a small retail centre. In addition, the Googong town centre will be a focal point for the region and include a variety of shops, cafés, restaurants, community facilities and commercial places, as well as housing apartments and townhouses.

Googong Township will progress in a series of neighbourhood stages over a period of around 20 to 25 years. The civil works at Googong began mid-2012 and the first housing construction developments commenced in early 2013.

The nearby Googong Foreshore area around Googong Dam will be managed as a separate water catchment, wildlife refuge and public recreation area.

#### 2.3.3 Australian Capital Territory

The Queanbeyan STP is located in the ACT and therefore has a broader regional context. While there is no pressure at present to develop the Queanbeyan STP as a regional facility, land development in the vicinity of the STP in the ACT could affect future decision making in respect of future planning for sewage treatment and disposal. Some of the more immediate developments that could affect future STP upgrades, include:

- Light industrial areas at Fyshwick and Hume
- Canberra airport
- Future development sites as identified in Figure 2-2
- The ageing Fyshwick STP facility
- Canberra development in the north including the Capital Metro plans
- Consideration of flows and runoff from Oaks Estate and Beard Estate.







#### Figure 2-1 Future development areas in Queanbeyan LGA

Queanbeyan Sewage Treatment Plant Masterplan Last saved; REV 5 / 22 September 2016







#### Figure 2-2 ACT Eastern broadacre development investigation areas

Queanbeyan Sewage Treatment Plant Masterplan Last saved; REV 5 / 22 September 2016





#### 2.4 Regional sewerage infrastructure

#### 2.4.1 Fyshwick STP

The Fyshwick Sewage Treatment Plant is located on approximately 32 hectares in the vicinity of the commercial and industrial areas at Fyshwick and the Jerrabomberra Wetlands. The plant treats sewage from the Majura, Fyshwick, Hume, Jerrabomberra and Narrabundah catchments, discharging the treated effluent to either:

- The Lower Molonglo Water Quality Control Centre (LMWQCC) for subsequent discharge to the Molonglo River downstream of Canberra, or
- The North Canberra Water Reclamation Plant for further treatment and subsequent use as recycled water for irrigation.

Icon Water prepared the "Canberra Sewerage Strategy (CSS) 2010-2060" report in response to the ACT population growth, changes in environmental conditions, foreseeable changes in government policies and community needs, and advances in treatment technology. The report aimed to identify and evaluate future treatment and discharge options for the Fyshwick STP site in the next 10 – 20 years.

The "CSS 2010-2060" report identified the following issues with Fyshwick STP:

- The Fyshwick plant was not able to handle peak wet weather flows during an event in December 2010 and capacity should be upgraded to 6 ML/d to handle such flow events
- There is leakage from lagoons to groundwater, as the lagoons are not completely sealed with an impervious base
- All sludge and a high proportion of the effluent is returned to the sewer for subsequent treatment at LMWQCC, which involves duplication of treatment effort and cost
- There is possible contamination of soils in some areas of the site, based on experience at similar treatment sites.

These issues are key drivers for service upgrade and Icon Water needs to decide the future of the Fyshwick STP - renew, replace or close. This decision remains with Icon Water but QPRC needs to consider it, given its proximity to the Queanbeyan STP. Fyshwick STP should be considered for a broader future regional solution to wastewater management.

A workshop in August 2015 aimed to formulate a best for region approach for sewerage management which considers the capacity and remaining asset life of the Fyshwick STP. An outcome of this workshop was an agreed governance structure for decision making in a regional context. An additional outcome of this workshop was a roadmap for collaboration and timely decision making that includes information gaps studies to support options analysis. This work is ongoing at the time of this Masterplan.

#### 2.4.2 The Lower Molonglo Water Quality Control Centre (LMWQCC)

The LMWQCC, located in the north west of the ACT, near West Belconnen is the main wastewater treatment plant for the ACT. The LMWQCC currently treats 80 ML/d of sewage from Canberra. Future upgrades to this plant have forecast an increase in capacity to 300 ML/d to accommodate future growth and wet weather flows.

The best for region workshop (August 2015) identified that flows from the ACT would continue to be treated at the LMWQCC and that, whilst the flow distribution may change, the altered flow regime would not fundamentally change the Queanbeyan STP upgrade.

#### 2.5 'Best for region' sewage treatment solution

Queanbeyan's location on the border of NSW and the ACT puts it in a unique position. The STP is located in the ACT on leased land and ACT Environment and Planning Directorate (EPD) (which includes the Environment





Protection and Water Regulation Division), ACT Health and the National Capital Authority (NCA) regulate various aspects of the STP operations1. The collection system network is located in NSW and QPRC is the service provider and is therefore regulated by the NSW Department of Primary Industries, Water Department (DPI Water).

During Phase 3 Masterplan and Feasibility of the QPRC STP Upgrade project, potential regional opportunities for wastewater management were discussed with the ACT Government and Icon Water. In May 2014 correspondence between QPRC and Icon Water identified a willingness to consider a regional solution for sewage treatment. During February 2015 a workshop was held with a range of stakeholders to outline the Draft Masterplan. In August 2015 a best for region solution was workshopped, with a framework for progress agreed between Icon Water, QPRC and the ACT Government (Particularly EPD and EDD).

In 2015 the interim ACT and Region Catchment Management Coordination Group was formed by the ACT Environment Minister. This group consists of multiple regulators and stakeholders including QPRC. The function of this committee is to implement an integrated catchment management approach in the ACT and Region, including improving water quality in Canberra's lakes (REF ACT Government Environment and Planning, 2014. ACT Water Strategy 2014-44 Striking the Balance. ACT Government Canberra, ACT).

<sup>1</sup> 

ACT EPA regulates discharges to the Molonglo River and NCA and ACT Health regulate discharges to Lake Burley Griffin from a water quality and human health perspective respectively, but only the ACT EPA issues a licence to operate the Queanbeyan STP





### 3 Future growth

To determine what quantum of flows need to be accommodated, projection of population growth was undertaken.

Population was determined from population statistics such as from census data as well as historical QPRC water usage data. The population values were then converted to equivalent population (EP) values to better account for the sewage inflows to be treated by the upgraded STP.

An EP calculator was developed to determine the EP (hence sewage flows) to be serviced by the upgraded plant over time. 28 existing and future urban areas were considered. Anticipated growth for the QPRC Local Government Area (LGA) was discussed with QPRC staff taking account of expected development nature, size and timing. This information was incorporated into the EP calculator and a series of maps was generated to show the likely growth areas and concentration of EP across the Queanbeyan LGA for Current, 10, 25 and 50 year horizons.

Further information about the EP calculator can be found in Appendix A.

#### 3.1 **Population projection**

Figure 3-1 shows the results of population projection generated by the EP Calculator and Table 3-1 shows the impact with and without the Googong Township which is served by its own STP. Five projections were generated:

- Lower bound limiting population
- Upper bound limiting population
- Lower bound expected population
- Upper bound expected population
- Population from EP considerations.

Population growth will result mostly from the nature of the expected release and construction of development areas, particularly in Googong and South Jerrabomberra. Planning is already well advanced for these developments and therefore growth is likely to occur in the early to middle period of the planning horizon.

This projects the total population for the Queanbeyan LGA prior to its amalgamation with Palerang. The population to be serviced by the STP Upgrade will depend on the staging and arrangement selected, i.e. all at existing site or decentralised.

Maps illustrating the growth concentration are shown in Appendix B.







#### Figure 3-1 Population projections for the Queanbeyan LGA

Table 3-1EP projection Inclusive / Exclusive of Googong as per EP Calculator projections					
Timeframe	Year	EP Excluding Googong	EP Including Googong		
Current	2015	45,737	45,917		
10 Years	2025	53,885	59,949		
25 Years	2040	76,972	92,535		

101,362

#### **Concluding observations** 3.2

2065

50 Years

The greater portion of growth is expected to occur in the middle part of the LGA within the 10 to 25-year horizon and in the southern part of the LGA within the 25 to 50-year horizon. Some low to moderate growth may occur in Queanbeyan Sewage Treatment Plant Masterplan Last saved; REV 5 / 22 September 2016

116,925





the middle part of the LGA (e.g. initial stage of South Tralee development) and as a result of urban infill over the next 10 to 15 years.

The first stage of the STP upgrade needs to provide sufficient time to address broader planning concerns as well as regional issues. Considering the population projection and other factors a planning horizon of about 10 to 15 years for the first stage seems appropriate. The first stage of the Queanbeyan STP Upgrade should allow for 60,000 EP to provide for 10 to 15 years' growth and in so doing:

- Address immediate needs in respect of existing STP condition and performance reliability, hence risk of not meeting discharge requirements
- Provide sufficient time to properly investigate longer term needs in respect of potential development in the LGA service provision
- Allow sufficient time to properly address regional cross border and other LGA planning issues.

It should be noted that these projections do not make allowance for ACT contribution to sewage flows, though depending on timing of possible ACT contributions some may be able to be accommodated.





### 4 Existing sewerage infrastructure

#### 4.1 Queanbeyan sewage collection network

The Queanbeyan STP services a catchment made up of urban and some rural residential properties, including the neighbourhoods of Crestwood, Jerrabomberra, Karabar, Queanbeyan, Queanbeyan East, Queanbeyan West and Rural East. Several pump stations within the catchment deliver flow to the STP via two independent trunk mains.

The STP treats sewage from the QPRC area and discharges treated effluent into the Molonglo River. It services all urban properties and some rural residential properties within the former Queanbeyan City Council area, the extent of which is displayed in Figure 4-1 and Figure 4-2. The Queanbeyan sewerage system consists of a gravity reticulation system with 19 pump stations and 280 km of pipeline. The capacity of the Queanbeyan STP existing treatment processes has been estimated to be around 34,500 EP (MWH, Dec 2008). The location of the STP is unique in that it also services a small urban area (Oaks Estate) in the ACT.

The existing STP receives flow from in and around the Queanbeyan area however, with the STP located in the ACT and relatively near the Fyshwick STP, future consideration could be given to possibly integrating the Queanbeyan and Fyshwick STPs in some way.

The Queanbeyan catchment area is anticipated to grow over the next 20 years with the development of the Googong and Tralee – Environa – Robin areas. Googong will be serviced by its own STP and a decision has yet to be made as to whether to service other areas by additional STPs. It is possible that the connected population to the Queanbeyan STP could grow considerably and therefore it is necessary to upgrade the STP to ensure effective treatment of current loads and to allow for the expected future population. This masterplan identifies this issue but does not seek to specifically address it.

#### 4.1.1 Collection system age and condition

Table 4-1 summarises the length (percentage) of sewers by age as well as the length of sewers that have been renewed to date. Sewerage infrastructure in Queanbeyan is ageing (with declining condition), with about 50% of the collection system older than 30 years. In addition, the collection system is also coming under increasing pressure from urban infill, which is expected to increase sewage flows in a system, which is already at or near capacity.

The effective service life of sewers is about 70 years. Consequently, there will be an increasing need to renew or replace the system over the next 10 to 20 years. A five year works program (2015 to 2020) identifies a further 21.25 km (about 6.5%) of gravity sewers to be renewed in order to maintain current service levels. The present rate of sewer renewals appears to be keeping pace with the rate of decline in condition and capacity. Flow gauging studies are being undertaken by QPRC to better understand flows in the system and to develop better strategies to reduce wet weather infiltration.

It is expected that sewer renewals and reduced wet weather infiltration will, in time, assist to provide additional system capacity for growth due to infill (in particular) and possibly to a lesser extent large urban development south of Queanbeyan.





Age of Sewer	Gravity Sewers				Pressure Ma	ins
	All (m)	Renewed (m)	% Renewed	All (m)	Renewed (m)	% Renewed
≤ 10 years	19,526	64	0.33%	398	0	0.00%
10 – 20 years	62,256	136	0.22%	1,979	0	0.00%
20 – 30 years	85,485	3,133	3.66%	784	0	0.00%
30 – 40 years	38,062	3,203	8.42%	1,049	0	0.00%
40 – 50 years	66,806	10,563	15.81%	0	0	0.00%
50 – 60 years	22,767	5,790	25.43%	135	0	0.00%
≥ 60 years	37,632	10,573	28.10%	0	0	0.00%
Total All Sewers	332,534	33,462	10.06%	4,345	0	0.00%

#### Table 4-1Length of Queanbeyan sewers renewed by age

Notes:

a) Data obtained from the Conquest Asset Register at January 2015

b) Shows the distribution of sewers by age

c) Shows the distribution of sewers by renewal.

#### 4.1.2 Collection system capacity

There is limited data about future infill development in Queanbeyan. This means that estimated growth rates for Queanbeyan are both general and qualitative. Current data suggests that growth due to infill is not likely to exceed 7,500 EP over the planning period of 50 years. Hence, any major extra load on the collection system is likely to be caused by new development south of Queanbeyan (e.g. South Jerrabomberra). Modelling of sewage flows in the existing urban area did not reveal any major issues. The only sewer likely to be affected is the DN 600 Jerrabomberra Trunk Sewer, which may be used to service land development south of Queanbeyan.

The Morisset St Pump station and Jerrabomberra trunk sewer are key pieces of infrastructure within the sewage collection system. Jerrabomberra trunk sewer would need augmentation to accommodate flow from additional land development. Morisset Street Pump Station has been inspected and some minor issues found. These should be addressed as part of the upgrade project.







#### Figure 4-1 Age of the QPRC LGA sewer network

Queanbeyan Sewage Treatment Plant Masterplan Last saved; REV 5 / 22 September 2016







#### Figure 4-2 Distribution of relined sewer mains in the QPRC LGA

Queanbeyan Sewage Treatment Plant Masterplan Last saved; REV 5 / 22 September 2016





#### 4.2 Sewage quality

A sampling program carried out by HWA and QCC (2011) found that the Queanbeyan inlet raw sewage at the STP inlet works resembled typical Australian domestic sewage. Notably, however, the Total Suspended Solids (TSS) 50<sup>th</sup> percentile for Queanbeyan STP is relatively high at 82 g/EP/d compared with typical domestic sewage TSS of 63 g/EP/d. This can be attributed to the high amount of limestone existing in the Queanbeyan area contributing a relatively high concentration of calcium. The per capita sewage load in Queanbeyan is estimated to be 226 L/EP/d and the peak wet weather flow factor is estimated to be 5.5 x ADWF. These values are considered typical of Australian domestic sewage systems.

The maturation lagoons have been in operation for over 40 years and are at the end of their operational life (investigation into structural integrity by HWA (2011)). Further, these lagoons lie below the level of the 1 in 100-year flood level and were damaged by the 1 in 20 year floods of 2010, leading to failure of Pond 2 embankment and release of around 30 ML of treated effluent plus additional pond sediment. This situation is a significant concern for ongoing operations as the ponds provide final polishing and disinfection of the treated effluent, and provide an effective buffer in times of high flow especially during wet weather events. Repair works have since remediated the flood damage. A Maturation Pond Management Plan has been developed and implemented to facilitate early detection and management of potential failures.

#### 4.3 Queanbeyan Sewage Treatment Plant (STP)

The STP has been upgraded a number of times in its eighty-five year lifespan, with its most recent upgrade occurring in the mid-1980s. The Queanbeyan STP was constructed in the mid-1930s, and is reaching the end of its service life. It has had a number of issues, which include:

- Structural failure
- Equipment obsolescence
- Maintenance issues
- Work health and safety (WHS) issues.

This STP was first commissioned in 1937 and since then has had three treatment trains added in upgrades. An outline of the current process train is provided in Figure 4-3. This process train is a mix of technologies patched together over time in reaction to capacity issues rather than a coherent integrated approach to meeting water quality objectives. Consequently, the process train needs to be refined. The following sections discuss the STP condition assessment. A full record of the condition assessment is presented in Appendix I. This assessment details the minimum suggested improvements for immediate attention, operation over the next 2 to 5 years and the possible refurbishment of parts of the STP for a 15 to 20-year lifespan, as part of a 60,000 EP plant upgrade.









#### 4.3.1 Inlet works

Two 12 mm screens are operated in duty and standby or bypass mode. The screens work on a flow based method and therefore not all inflows are screened. Due to the coarse nature of the screens a limited volume of screen material is actually removed from the process stream. A refurbishment was undertaken in 2014 in order to improve reliability. This entailed refurbishing the existing parts, adjusting the gearing ratio to 20%, checking the motor and reducing the bar aperture from 20 mm to 12 mm. Further influent screening improvements are needed to eliminate rags and coarse material from the treatment process. Rags enter the process train through the wide spacing of the bar screens on the inlet works. The rags contribute to high maintenance requirements for the biological filters, sludge tanks and lagoons.

The existing Vortex Grit Chamber appears to be in a satisfactory physical condition; however, the existing William Bobby cannot be used due to the hydraulic limitation of the inlet works. As a result, the primary grit chamber is not used and no grit removal occurs. Timber stopboards are currently used for flow splitting. The stopboards and penstocks are manually operated.

There is no influent overflow or bypass to a wet weather storage dam. Unauthorised flows to the environment are currently difficult to control during wet weather conditions. Given the likely trigger for new licence conditions or for a pollution reduction program to be applied by the NSW EPA should substantial upgrade of the plant be proposed; such a bypass would be expected as part of a future upgrade. The inlet works wet weather distribution arrangement requires operators to attend site since it is not an automated process. This may potentially lead to surcharge if the response time of operators is slow.




Based on the existing asset condition the minimum suggested improvements are:

- Screen all inflows
- Install smaller aperture screens (3-6 mm). Replace the raked bar screen with either a step screen or spiral sieve screen to capture a significantly higher volume of screenings
- Investigate and fix hydraulics to prevent overflows and hydraulic backup
- Replace the Vortex Grit Chamber as component of new inlet works as part of STP augmentation
- Consider the replacement of timber stopboards with more appropriate material and automated lifting to improve duty performance and WHS
- Install an influent overflow and storage bypass facility of sufficient volume to enable later treatment of bypass flows during high inflow events.

Given these, and considering the 60,000 EP plant upgrade, the recommended option for the inlet works is to construct a new inlet works with mechanical screens, grit removal, screenings and grit handling equipment and hydraulic flow distribution infrastructure

#### 4.3.2 Trickling filters

The four rock-media tricking filters are fed by rotating distribution arms, which are hydraulically propelled by the pressure of the incoming influent. There is no forced aeration; hence the units use very little energy. The trickling filters appear to be under-utilised both hydraulically and biologically, with no visible slime build up on the media surface.

Two of the trickle filters were installed in 1935 and show clear signs of structural deterioration with large cracks throughout the concrete structure. The concrete is in poor condition. The trickling filter walls were found to have moved off their foundations and managing to be held in place with the measures deployed such as steel prestressing cables.

Trickling filter effluent is pumped to the head of the secondary biological treatment zone (Trains 3 and 4), post the flow splitting zone. The water quality at this point is not known and therefore the process performance benefit of sending the trickling filter effluent through the secondary biological treatment is not clear. The use of trickling filters prior to secondary treatment may be impacting the Carbon : Nitrogen : Phosphorus ratio as well as causing hydraulic loading pressure on the secondary biological process (40% of the hydraulic load).

Based on the existing asset condition the minimum suggested improvements are:

- Consider decommissioning the TF1 and TF2 process train since all the effluent from this is routed through the Activated Sludge process train. Decommission to avoid catastrophic failure.
- Consider action to repair TF 3 and 4 if they are to be retained beyond five years.
- Conduct monitoring of the trickling filter effluent to assess if this can be re-routed direct to the maturation ponds. A portion of nutrient load and hydraulic load could at least be re-directed from the secondary process.

#### 4.3.3 Aeration tanks

There is no heating of air or water influent in the aeration tanks, limiting the efficacy of biological treatment in the cool climate conditions. Aerator speeds are controlled against the measured DO concentration set points by Variable Speed Drives (VSDs) fitted to the second and third aerators. Examination of historical dissolved oxygen and motor speed trends indicates that currently, the aerators are not controlling the dissolved oxygen levels as effectively as they could be. Aerator speeds appear to be almost constantly adjusting, and as a consequence the measured DO concentration in the aerated tanks is constantly changing (oscillating or overcorrecting).

Aerators are unable to maintain the required DO levels in the water. Aerator number 2 T1CH1 in particular appears to be in a deteriorated condition and underperforming.





Based on the existing asset condition the minimum suggested improvements are:

- Apply measures to aerate less either via SCADA / control / VSD adjustment / putting some aerators to 'off'
- Aeration zone should aim to be around 1.5 mg/L DO, although operator experience will dictate
- Possibly re-locate DO probes from being too close to the side wall and away from the aerator to get a better sensor placement
- Consider a retrofit 'cover' that could push the turbulence and DO transfer downward into the mixed liquor.

#### 4.3.4 Anaerobic digestion

The anoxic zones appear to have some turbulence (leading to air entrapment) due to poorly performing mixers. This air entrapment reduces the effectiveness of the anoxic nature of the zone, resulting in poorer nitrogen removal. Anecdotally the zones are not perceived to be anoxic and are too small to support their denitrification purpose, with TN high at around 14 mg/L.

Based on the existing asset condition the minimum suggested improvement is:

• Maintenance / refurbishment of the mixers as may be required to ensure air is not entrained and they operate efficiently.

#### 4.3.5 Clarifiers

The structural condition of the existing clarifiers is sound, with the concrete in all three clarifiers in good condition.

Uneven flow distribution is observed from the flow splitter chamber after the aeration tanks causing high solids loading to one of the settlement tanks. Currently the highly loaded Clarifier No.1 is cross-connected to the RAS Pump Station 2 to increase the re-circulation rate of return sludge and rectify the distribution issue. The RAS pumps, which consist of three ITT Flygt submersible pumps, also have uneven flow distribution causing high solid loading to RAS Pump Station 2.

Furthermore, as a result of the high levels of sludge that are carried in the aeration tanks (MLSS of 6,500 mg/L), there is noticeable carry over from the clarifiers to the Maturation Ponds which affect the effluent water quality.

Based on the existing asset condition the minimum suggested improvements are:

- Modify and extend the existing launder sprays to spray and break up the scum at the peripheral weir, and that the fixed brushes installed on the travelling bridge for weir cleaning are reinstated and maintained. This should help prevent scum clumping and accumulation at the weir. This should be fitted to each clarifier.
- Remove scum baffles and bridge scraper, allowing scum to enter Tertiary Lagoon inlet where it settles out instead of wasting at the clarifier, thereby re-entering the activated sludge system.
- Install new weir plates and accurate levelling of the plates.

#### 4.3.6 Maturation ponds

During the heavy rainfall in early December 2010, the No. 2 maturation pond embankment failed on the northern side of the pond. In view of the design standards for maturation ponds and the service life of the structures it was considered that the embankment had reached the effective end of its design life. It is possible there may be further failures in the ponds due to the inherent condition of the pond and the possibility of further extreme rain events. In regard to the future management strategy it is considered that some minor remedial works be undertaken in areas of high risk and that a formal surveillance program of the embankments be implemented.

There is a level of algae actively within the maturation ponds which affects the effluent water quality. This is largely attributed to the 40 years of silt accumulation in the pond. The algal activity within the ponds results in changing bicarbonate concentrations and a rise in TDS, associated with seasonal algal blooms. This is also linked with the change in pH, which has exceeded the limits for the STP.





These dynamic processes within the maturation pond result in poor water quality and insufficiently disinfected effluent. The ponds have been fitted with aerators however these have not been used for years. The performance and condition of the aerators in the maturation ponds has not been described.

Based on the existing asset condition the minimum suggested improvement is:

• Undertake a risk assessment for the inlet tertiary lagoon facility. It is anticipated that as a minimum, the risk assessment recommendations would include a requirement for fencing around the perimeter of the inlet lagoon, together with warning signs alerting personnel to the hazards upon entering the fenced area.

Given the improvements identified for the existing secondary treatments, and considering the 60,000 EP plant upgrade, the recommended option for the secondary treatment process involves a MBR or conventional activated sludge process using best biological design principles with combined biological / chemical phosphorus removal, single sludge stream and aerobic sludge digestion.

## 4.3.7 Sludge handling system

Sludge from the activated sludge process is wasted to one of two lagoons, where it is stored and stabilised prior to drying on the site's sludge drying beds. Only one of the sludge lagoons is fed over a period of typically 6 to12 months, whilst the other is retained on standby. After this time period, which allows for settling and partial dewatering, partially dewatered sludge is placed onto drying beds. The sludge lagoons are at capacity, with both lagoons full to near overtopping. In a storm event, an environmental incident could result due to lagoon volume and lack of alternate options for storage.

In addition, the sludge drying beds are at capacity causing a backlog of waste in the lagoons. The stockpile area is also at capacity and an alternative is required in the short-term.

Based on the existing asset condition the minimum suggested improvements are:

- Review operations and hydraulics to ascertain root cause of both lagoons being substantially full. Based on this review determine options to mitigate.
- Undertake mechanical dewatering of sludge drawn from the lagoons (possibly utilising mobile dewatering equipment) to enable the sludge drying beds to be bypassed, or the loading on the sludge drying beds to be significantly increased.
- Consider disposing of dewatered cake (14 to 17% solids) to a future waste sludge cake receival facility, or direct to the sludge drying beds for further drying.
- Establish additional drying beds.
- Consider sludge dewatering equipment including a screw press, belt filter press or centrifuge.

Considering the 60,000 EP plant upgrade, the two options considered for upgrading the sludge dewatering facility are either:

- Expansion of the existing manually operated drying beds
- Construction of a new mechanical dewatering facility incorporating either: centrifuge or belt filter press equipment, polymer dosing system and sludge out-loading infrastructure.

#### 4.3.8 Electricals and motors

The majority of the STP components need to be replaced or rehabilitated. The majority of the electrical controls and electrical equipment is described as obsolete.

The motors throughout the Queanbeyan STP are described as aged, inefficient and have a reduced lifespan. This was indicated by the electrical investigation by KMH Electrical in 2012. The motors are identified as relatively small for their operations. The continuous high load on the motors throughout the plant had caused them to age and the motors are expected to be nearing the end of their operational lifespan.





Other instruments such as flowmeters are non-operational, and if functioning not calibrated.

The adjustment of penstocks is not automated.

### 4.3.9 Civil structures

A large proportion of the original treatment plant is still integral to the current treatment process. Civil structures associated with the original plant show a lot of wear and tear, which is understandable with exposure to harsh conditions over a long period. This is demonstrated by the extensive cracking around the trickling filters that are now post tensioned (braced) with steel cabling. Other concrete structures show similar signs of deterioration and the structural integrity of pipework around the cold digester arrangement is in a state of disrepair. It is unlikely any of the structures meet current standards (water retaining structures, earthquake loading, WH&S etc.) and as such represents a considerable legal / liability risk for Council. The remaining life of the ageing infrastructure is questionable, given its current age and there will be a substantial cost in refurbishing and maintaining the aged assets, albeit for a reduced lifespan (15 - 20 years) when compared with new infrastructure.

Cost estimates for the repair and refurbishment of treatment components that are required to support operation immediately and in the short term (2 - 5 years) are presented in Appendix I.

### 4.3.10 Existing authorisation

The Queanbeyan STP is currently certified under the Environment Protection Act 1997 (Environmental Authorisation 0417). The general requirements of this authorisation include:

- General water protection conditions
- Monitoring
- Reporting
- General conditions for diversion to the lagoons
- Management of sludge.

The ACT Environmental Protection Authority (EPA) has previously supported the proposed STP upgrade under the conditions of "no pollutant increase" (letter, Lucy Vincent (EPA) to Greg Fogarty (QPRC), 13 November 2008).

The operations of the whole sewerage system (STP and collection system) comes under the jurisdiction of DPI Water, which carries out periodic inspections of the STP. This means that the regulatory context for the STP operations is complex.

A new licence would be required as a result of this upgrade project.

## 4.4 Concluding observations

With an ageing plant, operability and reliability present a number of challenges, largely relating to operator involvement. The key issues are as follows:

- Work Health and Safety (WHS) risks exist as a result of aged infrastructure and manual operation of stopboards and penstocks
- · Hydraulic capacity issues and treatment inefficiency for the inlet works and primary screening
- · Environmental discharges of untreated stormflows in the absence of stormflow storage
- The treatment train has been developed in a somewhat adhoc approach, with adjustments being made to the original STP components. The current treatment train could be improved to enhance treatment and operability
- The sludge handling facilities are undersized and sludge treatment could be enhanced





- Most equipment throughout the STP is manually controlled with limited feedback into the plant SCADA system; hence not all equipment failures are detected for response
- Most of the STP mechanical and electrical plant / equipment is at the end of its effective life and needs replacement.

The existing Queanbeyan STP condition currently presents a risk to QPRC with numerous suggestions for both immediate and short-term improvement. Beyond operability and WHS issues, there will be a stronger focus on water quality and environmental discharges. Tighter discharge criteria are likely to be imposed in the future when licence conditions are re-negotiated. Following a workshop for this project, Heath Chester (ACT EPA) commented "Queanbeyan *STP effectively sets the baseline of the nutrient status for Lake Burley Griffin, thus any reduction in nutrient input from the STP will assist the River and Lake in being more resilient to other stressors"*. Whilst diffuse nutrient pollution of the River and Lake present a highly important contribution of nutrients to these waterways, the Queanbeyan STP presents the highest known point source discharge of nutrients within the catchment and thus improvements in treatment will be a target for the Catchment Management Co-ordination Group and will ultimately be of value to the receiving waterways.

Given the advances in treatment technology, the age and condition of the existing STP, and the likely more stringent future effluent discharge requirements, the appropriate course of action for QPRC is to upgrade the existing STP, potentially replacing it completely. Table 4-2 presents the short and long-term options for the treatment. Many treatments need immediate intervention and short-term refurbishment to sustain the existing plant operation. Most are unfit or unable to be adapted to be functional within the scheme of the new 60,000 EP STP. Comments are provided to this effect.

Given the treatment limitations the most obvious option for consideration is full replacement. The other options include some re-use of existing assets where they can be retained and refurbished to a 25-year lifespan. The benefits of full refurbishment are as follows

- Better assurance that completed works will meet required discharge requirements
- Better assurance that completed works will have an adequate service life over and above additional service life that might be achieved through renewing or retrofitting the existing plant
- Easier and less risk during commissioning and transfer of operations to the new plant (the existing STP can be kept in operation while commissioning and proving the new STP)
- The ability to accommodate future increased loads due to growth, particularly in the south of the LGA.





### Table 4-2Short and long term options for treatments

Area	Outcome	Comment	Outcome	Comment
	(2-5 years)		(15-25 years)	
Inlet screens	Refurbish	For interim service only	Redundant	Outdated and undersized process unit and would serve no purpose in a new or updated plant
Inlet flow splitting and flumes	Refurbish	For interim service only	Redundant	• Outdated and undersized process unit and would serve no purpose in a new or updated plant
Aerated grit chamber	Retain – performing no role	For interim service only	Redundant	Undersized and underperforming process unit and would serve no purpose in a new or updated plant
Vortex grit chamber	Refurbish	For interim service only	Redundant	Undersized and underperforming process unit and would serve no purpose in a new or updated plant
Primary clarifier and Imhoff tanks	Retain	<ul> <li>Imhoff tanks outdated process unit</li> <li>Structures/concrete in very poor to fair condition</li> <li>Primary solids removal not consistent with an improved environmental discharge of &lt; 5 mg/L TN as want to retain carbon</li> <li>Limited to no residual design life</li> <li>Not compliant with WHS standards.</li> </ul>	Redundant	<ul> <li>Limited possibilities in refurbished or new plant options:</li> <li>Inlet flow balancing volume (for MBR using existing bioreactors)</li> <li>Solids removal for part load</li> <li>Standby emergency storage unit.</li> </ul>





Area	Outcome (2-5 years)	Comment	Outcome (15-25 years)	Comment
Trickling Filters 1 and 2	Retain (monitor closely for catastrophic failure). Bypass if other secondary treatment is sufficient.	<ul> <li>Structures/concrete in fair to poor condition</li> <li>Poor location – Low elevation</li> <li>Not consistent with an improved environmental discharge of &lt; 5 mg/L TN.</li> </ul>	Redundant	<ul> <li>Trickling filter outdated process unit and would serve no purpose in a new or updated plant.</li> </ul>
Trickling Filters 3 and 4	Retain	As above.	Redundant	As above
Secondary reactors	Retain (some possible refurbishment / improvements to process aspects)	<ul> <li>Structures / Concrete generally good condition</li> <li>Residual design life not clear</li> <li>Difficult construction and operation staging – likely to increase timeline by 18 to 24 months as cannot be taken fully offline</li> <li>Trapezoidal base difficult to retrofit diffused aeration</li> <li>Down-rate would require retrofit to meet TN &lt; 5 mg/L.</li> </ul>	Refurbish / Redundant (dependant on concept design and hydraulic cycle) (concrete may not have sufficient residual design life).	<ul> <li>Possibilities for use in refurbished or new plant as:</li> <li>Aerobic digester (2 – 2.5 ML required) and existing aeration maybe OK - to achieve Grade B Biosolids</li> <li>Balance volume for MBR plant - either new plant or combined with refurbishment (6 – 8 ML required)</li> <li>Bioreactor in MBR process (6 - 7 ML required) – challenge to refurbish/ reconfigure and maintain treatment</li> </ul>





Area	Outcome (2-5 years)	Comment	Outcome (15-25 years)	Comment
Humus clarifier and tank	Retain	<ul> <li>Structures/concrete in fair condition</li> <li>Poor location – low elevation = pumping costs to downstream process step</li> <li>Limited to no residual design life</li> <li>Not compliant with WHS.</li> </ul>	Redundant	<ul> <li>Treatment would serve no purpose in a new or refurbished plant</li> <li>Too small to be much significant use in future plant as a tank for an alternate use.</li> </ul>
Clarifiers	Retain	<ul> <li>Structure/concrete in good condition</li> <li>Poor flow split between tanks</li> <li>Chain scrapers: very old technology</li> <li>Weirs and scum baffles/skimmers require replacement</li> <li>Poor position – Low elevation and close to flood level (unless effluent lagoons reused) – need to pump to tertiary process step to achieve a potential future TP target of &lt; 0.1 mg/L.</li> <li>Suspect foundation encroachment from flood inundation.</li> </ul>	Refurbish, including flow splitter (dependant on concept design and hydraulic profile)	<ul> <li>Possibility to reuse as tertiary clarifiers to settle chemical P solids</li> <li>Would require significant mechanical retrofit to achieve performance required – difficult in the shape of clarifier</li> </ul>
Anaerobic digester	Redundant	-	Redundant	





Area	Outcome (2-5 years)	Comment	Outcome (15-25 years)	Comment
Maturation Ponds	Retain (possible vegetation removal)	<ul> <li>Structures in poor to fair condition and require substantial retrofit and refurbishment to achieve performance</li> <li>Concern about long-term stability of creek-side embankments</li> <li>Below flood level – retention may require a flood levee bank be constructed</li> <li>Outlet for environmental discharge is impacted hydraulically by the Molonglo River water level.</li> </ul>	Refurbish / Redundant (dependant on concept design and hydraulic profile)	<ul> <li>Possibilities for use in refurbished or new plant options:</li> <li>Effluent polishing and solids removal with use of secondary clarifiers in tertiary clarifier duty</li> </ul>
Sludge lagoons	Refurbish plus additional lagoon	<ul> <li>Struggle to meet current performance due to size as sludge is not pre thickened</li> <li>Not compliant with WHS standards.</li> </ul>	Refurbish / Redundant (Dependant on concept design and hydraulic profile).	<ul> <li>With WAS pre-thickened to 4.5% DS - Provides 80 days in each lagoon.</li> <li>Possible to therefore use in refurbished or new plant to achieve Grade B biosolids.</li> </ul>
Sludge drying beds	Refurbish plus additional bed	-	Refurbish / Redundant (dependant on concept design and hydraulic profile).	Possible to use in refurbished or new plant.





Area	Outcome	Comment	Outcome	Comment
	(2-5 years)		(15-25 years)	
Bypass storage lagoon	New facility proposed	-	Retain.	Possible to therefore use in refurbished or new plant.
Buildings - all	Refurbish (limited)	-	Refurbish / Redundant (dependant on concept design).	Possible to therefore use in refurbished or new plant.





# 5 Future sewerage infrastructure

## 5.1 South Jerrabomberra

Significant development is planned for the South Jerrabomberra valley, located to the South East of Queanbeyan Central Business District, as shown in Figure 5-1. In the first stage of development, this area will be served by a sewage pump station (SPS) to transport sewage to the Jerrabomberra Trunk Sewer (hence Queanbeyan STP). In the future, an upgraded SPS and Jerrabomberra Trunk Sewer or an independent STP could serve the area. It is possible that unplanned discharge to the Jerrabomberra Creek system could occur from sewerage infrastructure constructed to service this area in the short term. Depending on future planning decisions about servicing the South Jerrabomberra area there may be a need to allow for planned licensed discharges of treated effluent.



Figure 5-1 Proposed future land uses of South Jerrabomberra





Sewage from the development will need to be treated either by the Queanbeyan STP (via the Jerrabomberra Trunk Sewer) or a future local decentralised STP.

A pump station at the northern end of South Tralee has been proposed to service the initial stage of this development. An additional independent pump station may be needed to service the northern developments of Environa, North Tralee and Poplars.

The existing telemetry system is unable to communicate reliably with these proposed pump stations and will therefore need to be upgraded. Upgrading of the telemetry systems should be considered as part of the first stage of upgrading the existing STP.

The 600 mm diameter Jerrabomberra Trunk Sewer could potentially be used to drain major developments to the south of the Queanbeyan urban area. The impact from new developments (viz. Tralee) and urban infill on the trunk sewer was analysed using XPSWMM software. This software tracks sewage flows as they progress downstream taking into account storage effects within the pipe network.

The model for the STP Masterplan was developed in conjunction with planning for the South Jerrabomberra / Tralee developments. These investigations indicated that the optimum point of connection for future loads is manhole W76 on the Jerrabomberra Trunk Sewer. The computer modelling assumed that future developments south of Tralee would also be connected at manhole W76.

Although the model provides a reasonable snapshot of likely flow conditions, a more detailed analysis will be needed during concept design to confirm results and provide sufficient basis for design of future augmentations. The criteria used to identify problem areas in the Jerrabomberra Trunk Sewer are listed in Table 5-1 and loads on the trunk sewer used to calculate flow conditions are listed in Table 5-2. It should be noted that the average dry weather flow (ADWF) used in this capacity assessment is more conservative than the value derived for the growth projections (refer Section 3). This was done to account for uncertainties about future conditions.

Item	Description	Value
ADWF (for existing urban areas)	Daily dry weather discharge from an equivalent person. This includes a minor allowance for dry weather ground water infiltration. The given value is based on experience in the existing sewerage network and makes allowance for declining sewer condition over time and also takes into account increased base flows due to deterioration of private sewers.	240 L/EP/day
ADWF (for future urban areas)	Daily dry weather discharge from an equivalent person. This includes a minor allowance for dry weather ground water infiltration. The given value is based on data related to new developments being planned for Googong and Tralee. A lower per capita discharge was assumed in these areas because the designs will be based on newer technology, low infiltration design and construction methods, and water efficient approaches.	210 L/EP/day
Peak dry weather flow (PDWF / ADWF) ratio	The software uses flow hydrographs (diurnal flow variation) as an input instead of a multiplier. The ratio of the peak value to ADWF in the model is indicated. The diurnal pattern (attached) was based on data from similar catchments as Queanbeyan does not have any gauged data.	2.20

## Table 5-1 Sewer Capacity Criteria





Item	Description	Value
Peak wet weather flow (PWWF / ADWF) ratio	Wet weather events were not modelled as there was limited hydrologic data. However, flows into the STP indicate that the ratio of wet weather flow to average dry weather flow is in the order of 5.50. This ratio was used together with the dry weather modelling results to assess the risk of overflows from the system.	5.50
PDWF / Qf ratio	Wet weather flows up to a design event are usually contained within the pipe barrel i.e. the pipe capacity (Qf) must be equal to the PWWF. This means that the PDWF must be limited in order to provide sufficient capacity for wet weather ingress. The value given is based on current data for Queanbeyan.	0.40
d/D ratio at PDWF	This ratio value is a direct result of circular pipe hydraulics and the PDWF/Qf ratio of 0.40.	0.44
Vsc	The generally accepted self-cleaning velocity (minimum) at PDWF for sewers is 0.70 m/s. This provides flow conditions in the sewer, which will transport solids along the sewer rather than allow solids to settle and build up in the sewer.	0.70

#### Table 5-2 Sewage Loads on the Jerrabomberra trunk sewer

Planning Horizon	Queanbeyan		Future Urban Areas		Total Development	
	EP	ADWF (ML/d)	EP	ADWF (ML/d)	EP	ADWF (ML/d)
Current	42,924	10.30	2,100	0.50	45,024	10.81
Yr 10 - Ca. 2025	44,362	10.64	7,488	1.73	51,850	12.44
Yr 25 - Ca. 2040	46,609	11.20	26,678	6.39	73,287	17.59
Yr 50 - Ca. 2065	50,611	12.15	43,837	10.52	94,448	22.67

Notes:

1) The estimate of EP (effective population) and sewage flows was based on EP projections prepared for this Masterplan (refer Section 3).

2) Growth in existing urban areas was assumed to be about 0.33% per annum.





Table 5-3 shows the outcomes of the analysis of the expected growth in sewage flows.

### Table 5-3Outcomes of analysis

Year	Comment / Observation	Length (m)
Current	There appears to be sufficient capacity in the trunk sewer for current loads and the sewer appears to operate within appropriate hydraulic standards. However, some surcharging of manholes in the lower reaches is likely to occur during wet weather events.	(W78-IC) 6,953
Yr 10 - Ca. 2025	The trunk sewer between manholes W78 and W34 appears to have sufficient capacity for expected loads and operate within appropriate hydraulic standards.	(W78-W34) 4,383
	Between manholes W34 and W1 the sewer exhibited surcharging of manholes and there appeared to be a high risk of overflow between manholes W8 and the STP inlet channel.	W1 – W34 2,575 m W8 – STP 635 m
	The extent of surcharging between manholes W34 and W8 was not considered significant. Accepting a lower operating standard for this section could be used to delay major investments in upgrading the capacity of the sewer.	
Yr 25 - Ca. 2040	The trunk sewer does not have sufficient capacity for the expected Year 25 loads and there appeared to be a significant risk of overflow at a number of points along its length.	6,652 m
Yr 50 - Ca. 2065	The trunk sewer does not have sufficient capacity for the expected Year 25 loads and there appeared to be a significant risk of overflow at a number of points along its length.	6,652 m
Notes:		

1) Analysis assumes the whole of any additional loads from future development will be transferred to the Jerrabomberra Trunk Sewer at Manhole W76

2) Figure 5-2 (following) shows the affected sections of the Trunk Sewer due to expected Year 10 loads.







Figure 5-2 Expected condition of the Jerrabomberra trunk sewer after 10 years (Image from South Jerrabomberra Structure Plan 2013)





# 5.2 Googong Township

Googong Township is designed around an integrated water cycle (IWC), which aims to cut potable water consumption by up to 60%. The IWC includes all elements associated with the supply of potable water, the collection and treatment of sewage flows and transfer of treated flows into the recycled water system for reuse in the community. The system includes potable water, recycled water and sewerage collection networks (collectively known as the Network) and a Water Recycling Plant (WRP).

The Googong Township IWC infrastructure comprises of the following:

- The WRP
- Reservoirs for recycled and potable water
- Pump stations for sewage, recycled water and potable water
- · Mains pipework for sewage, recycled water and potable water to connect to the neighbourhoods
- Structure for the discharge to the stormwater management system
- An Interim Sewer Service was implemented to provide a sewer service for the initial occupancies in the development.

As a result of the IWC arrangements, sewage flows from the area will not drain to the Queanbeyan system, hence have been disregarded in assessing future flows for the proposed Queanbeyan STP upgrade. In contrast, the Googong STP makes no provision for solids treatment and disposal. Hence, solids from the Googong WRP will need to be considered in developing a solids management strategy for the Queanbeyan Palerang LGA.

## 5.3 Concluding observations

A summary of the risks associated with not upgrading the existing trunk main and the existing hydraulic capacity of treatment at Queanbeyan are presented in Table 5-4. This includes the risk of development in the South Jerrabomberra area being delayed, or alternatively being accommodated without capacity, resulting in environmental and public health consequences.

Development Risk	Environmental Risk	Public Health Risk	Economic risk	Reputational Risk
<ul> <li>Risk expansion cannot occur due to capacity constraint</li> <li>Risk expansion will occur regardless of capacity due to political and developer pressure.</li> </ul>	<ul> <li>Risk of discharge from the trunk main</li> <li>Risk of bypass overflow and inadequate treatment, resulting in poor water quality downstream</li> <li>Sludge handling risk of being unable to manage increased sludge loads, resulting in an environmental incident or trucking off-site.</li> </ul>	<ul> <li>Risk of direct contact with discharge from the trunk main</li> <li>Resulting public health risk to downstream Queanbeyan River users.</li> </ul>	<ul> <li>Loss of potential revenue if Council constrains development</li> <li>Financial cost of environmental breeches</li> <li>Cost of sludge handling and disposal outside of the LGA.</li> </ul>	• Risk to the reputation of Council through constrained development.

## Table 5-4 Summary of risks





It is recommended that:

- The South Jerrabomberra sewer trunk will need to be upgraded to meet future capacity:
  - Consider augmentation of the Jerrabomberra Trunk Sewer between manholes W8 and the inlet channel of the STP
  - Any further augmentation should be delayed until a final service strategy is decided for future development to the south of Queanbeyan
  - A survey and sewer gauging program should be implemented for the whole length of the trunk sewer (manhole W78 to the STP inlet channel) to enable a more detailed analysis of the sewer
- Continue discussions with Icon Water around cross-border arrangements and a regional approach to sewage management.
- A septic tank receival station should be included in the new plant.





# 6 Environmental constraints

There are environmental constraints in the QPRC LGA that could potentially affect future construction and expansion in the region. This must be addressed when considering the location of sewage infrastructure. The more important criteria are discussed further below.

## 6.1 Heritage reserve

Land that is listed as heritage protected will have particular restrictions regarding construction in the area such as the type of structure that can be erected, restriction on removal of vegetation to accommodate for space for a new STP etc. Particular care must be taken to meet these requirements, and so this will affect population growth in the regions displayed in Figure 6-1.



Figure 6-1 Heritage reserve areas in the QPRC LGA





# 6.2 Scenic protection

Canberra government enforces restrictions in order to protect the aesthetic integrity of regions considered scenic. This will affect projects that would require significant landscaping or that would obstruct scenic views. Areas under scenic protection are displayed in Figure 6-2.



Figure 6-2 Scenic protection areas in the QPRC LGA





## 6.3 Quarry buffer

The Holcim quarry is located west of Googong, as shown in Figure 6-3. This buffer area is required to be maintained and cannot be encroached on by development.



Figure 6-3 Quarry buffer area in the QPRC LGA





# 6.4 Australian Noise Exposure Forecast (ANEF)

Canberra Airport is situated north west of Queanbeyan giving rise to flight paths directly over the western portion of the LGA. Figure 6-4 displays the noise effects caused by the nearby airport on the Queanbeyan LGA.

ANEF modelling produces a noise exposure (ANEF) map showing contours for 20, 25, 30, 35 and 40 ANEF units. Higher contour numbers represent greater cumulative amounts of aircraft noise over an average one-year period. ANEF units are not decibel measurements - they are measures of adverse community reaction to aircraft noise. Above 20 ANEF homes, schools, hospitals and nursing homes should have noise insulation and above 25 ANEF, aircraft noise is too great for these buildings even with insulation. Even at 15 ANEF, 35% of people are seriously or moderately affected by aircraft noise. ANEF of less than 20 is acceptable for the building of new residential dwellings.



Figure 6-4 ANEF for airport noise levels in the QPRC LGA





## 6.5 Floodplains

Rainfall in the area flows from the surrounding mountain ranges towards Queanbeyan River, which runs from the Googong reservoir, down through Karabar / Greenleigh, towards Queanbeyan where it merges with the Molonglo River. The area at the bottom of the Queanbeyan River, where it merges with Molonglo, is at risk of flooding, as illustrated in Figure 6-5.



## Figure 6-5 Floodplain areas in the QPRC LGA

Flooding is an issue at the existing site. Figure 6-6 shows (in yellow) the Q100 flood line for the existing STP site. The river is shown schematically in blue, and the main STP process assets are outlined in green. Any future work will need to ensure that the infrastructure is protected from the Q100 flood, and that any existing infrastructure that lies within the Q100 is decommissioned appropriately.







Figure 6-6 Contour of Q100 flood line in relation to Queanbeyan STP infrastructure





## 6.6 Bushfire prone areas

Although the Queanbeyan suburbs are densely populated, the majority of the LGA is significantly vegetated. These areas are quite bushfire prone, especially in the north-eastern mountain ranges. Figure 6-7 indicates the possible bush-fire risk level throughout the LGA; as linked to the vegetation category being proportional to the bushfire risk level.



Figure 6-7 Areas in the QPRC LGA with significant bushfire risk





## 6.7 Review of current site

A preliminary review of the environmental aspects considering constraints and issues for the current site has been undertaken. Consideration has also been given to how some of these issues can be managed. The results of this review are given in Table 6-1.

### Table 6-1 Current site environmental aspects and potential mitigation

Environmental Aspect	Potential Mitigation
Odour	<i>Issue</i> The nearest sensitive receptor is at the south-eastern boundary of the site in Oaks Estate and Beard Estate. All possible measures would need to be considered to reduce the emission of odours that could potentially affect sensitive receptors. Wind and other meteorological aspects need to be determined to assess their effect on potential odour emission. No conditions exist in the Licence. <i>Mitigation</i> Liaison with stakeholders should occur to determine if odour emissions are occurring. Considerations should be taken for any activity during construction which could increase the levels of odour emissions.
Noise and Vibration	<ul> <li>Issue</li> <li>All reasonable steps would need to be taken to reduce construction equipment noise and minimise impact on neighbouring properties. The nearest sensitive receptor is at the south-eastern boundary of the site.</li> <li>Mitigation</li> <li>Construction activities would be restricted to certain times of the day, e.g. Monday to Friday 7 am – 6 pm, Saturday 8 am to 1 pm. No work would be undertaken on Sundays or public holidays.</li> <li>Equipment selection and design should consider noise impact implications. Blowers and other potentially noisy equipment could be housed in suitably designed buildings to provide noise attenuation.</li> </ul>
Transport and Traffic	<i>Issue</i> There would likely be an increase in traffic to the site during construction works; including construction vehicles, deliveries and construction personnel travelling to and from site. This could lead to a large amount of congestion, resulting in a disruption to other transport routes. Further, the extra traffic may increase the possibility of erosion along road-sides. <i>Mitigation</i> Speed limits should be adjusted to manage traffic appropriately. There should also be an increase in road signage. Machinery should be maintained and checked to be in working order. Further, road load limits and sight distances should be taken into consideration when formulating a traffic management plan. The approach roads to the plant will need to be upgraded.
Chemical Handling	<ul> <li>Issue</li> <li>There is potential during construction and operation for the occurrence of spills and leaks. This could potentially contaminate soil and waterways. Further, the health of fauna, flora, and humans could be adversely affected.</li> <li>Mitigation</li> <li>Designated areas should be determined to accommodate potentially damaging materials. The storage and handling of chemicals should be in accordance with the safety data sheet and other guidelines. There should be appropriate procedures and emergency plans in place, and these plans should be included in staff inductions and training.</li> </ul>





Environmental Aspect	Potential Mitigation
Sludge Handling	<i>Issue</i> Large amounts of contaminated material (in the form of sludge) would be produced during operational activities. If managed inappropriately, this could contaminate local waterways and soil. Section 3 of the Licence indicates that sewage sludge and screenings should be managed on site such that there is no discharge to surface water or groundwater. It is anticipated that in the new plant, this practice would not be allowed to continue but instead treatment and disposal should occur. Reuse of sewage sludge in the ACT should be in accordance with the National Water Quality Management Strategy Draft Guidelines for Sewage Systems Sludge (Biosolids). <i>Mitigation</i> Proper disposal methods and safety plans should be designed and incorporated into staff inductions and training. The design of systems that produce sludge should allow for safe removal.
Land Use	<i>Issue</i> The site is an existing STP and this use would continue under this project. There are adjacent land users who may be affected by construction or operational impacts. <i>Mitigation</i> Appropriate liaison with the different stakeholders to maintain open and clear communication channels should be incorporated. An allowance for stakeholder feedback would also assist mitigation.
Soil Contamination	Issue There is known contamination on the site due to burial of solids and screenings. Mitigation Consider location of new works to avoid contaminated areas. Provide for remediation in the scope of works for construction.
Flora and Fauna	<ul> <li>Issue The STP site is not likely to be a habitat for any threatened species (though this needs to be checked during the EIS) and therefore it is unlikely that the proposed construction works at the site will have an impact on any threatened species. Threatened ecological communities listed in the EPBC Act should be considered. Those communities which are likely to occur are: <ul> <li>Natural Temperate Grasslands of the Southern Tablelands of NSW and the ACT (Endangered)</li> <li>White Box-Yellow Box-Blakely's Red Gum Grassy Woodland and Derived Native Grassland (Critically Endangered). </li> <li>Consideration should also be given to ecological communities that may be present in the maturation lagoons.</li> <li>Mitigation</li> <li>Tree removal would be minimised in design. Environmental management plans would be required for construction and operation stages. </li> </ul></li></ul>





Environmental Aspect	Potential Mitigation
Air Quality	Issue
	Local air quality could be affected by emissions from construction traffic and equipment. Earthworks required as part of the construction works may give rise to dust impacts. It is not anticipated that there will be long-term impacts on air quality from the operation of the STP.
	Mitigation
	Construction vehicles and equipment would be required to have been serviced within the six-month period prior to the commencement of construction activities;
	Limit the area of bare ground to be exposed at any one time (where possible);
	Water down bare ground during construction, particularly during windy conditions.
Water Quality	Issue
	Operationally the proposed upgrades to the plant will improve treated effluent quality and therefore reduce the potential impacts of effluent leaving the site. Impacts to water quality could arise during construction due to sediment run-off. The Licence indicates various load limits for pollutants.
	Mitigation
	A project specific construction environmental management plan would be prepared prior to construction commencement. In maintaining current environmental flow levels, a monitoring system will need to be put in place. Further, effluent quality will still need to be monitored to minimise the risk of contamination in the effluent.
	Design phase should consider river bank restoration and protection to guard against flood damage and spills from ponds.

## 6.8 Concluding observations

The following measures should be considered when deciding the location of the future STP:

- Avoid heritage listed sites, scenic protection areas, and quarry buffer zone
- Construction within the ANEF affected areas could be considered appropriate as aircraft noise is unlikely to be an adverse impact on STP operations
- Avoid infrastructure within the Q100 flood level without adequate flood protection measures in place
- Avoid bushfire prone areas or provide adequate protections, appropriate to STP operations
- Consider and incorporate mitigation of environmental issues (such as water quality, odour, noise, contaminated land etc.) on existing site as part of concept design.





# 7 Water quality objectives assessment

# 7.1 Scope

A water quality objective assessment (WQOA) was undertaken to investigate, model and examine the effects of current and future STP operations on receiving water quality for a range of possible treatment, effluent quality and release scenarios. The outcomes from this study were used to inform the development of future effluent quality objectives which in turn will influence decisions on treatment options, technologies and operations of the new STP. Water quality and flow data analyses have been undertaken to understand the present and historical conditions in the Molonglo River and in Jerrabomberra Creek, and how these may have been influenced by the STP.

The data analysis was used to inform and develop detailed models of the Molonglo River quality in the reach from the present STP discharge location to Lake Burley Griffin (LBG). The model was then used to understand the 'baseline' water quality of the river in the hypothetical absence of any STP discharging into the river. This baseline was superimposed with several test scenarios for various future STP loading, effluent quality and flow rate permutations to understand the impacts that future plant operations may have on receiving water quality. It is anticipated that the model outcomes will inform a discussion on future effluent quality and Molonglo River management objectives. The effluent discharge and water quality scenarios reviewed are summarised in Table 7-1, at the Locations as shown in Figure 7-1.

For the full report, refer to Appendix D.

Scenario	Equivalent Population (EP)	Discharge (m³/s)	Total Nitrogen (mg/L)	Total Phosphorus (mg/L)	Faecal Coliforms (CFU/100 mL)
1	0 (i.e. no STP)	0	N/A	N/A	N/A
2	45,000 (current)	0.133	5	0.1	Time series generated from
3	45,000 (current)	0.133	10	0.2	distribution to historical
4	45,000 (current)	0.133	15	0.3	effluent data and random sampling (log mean = 3.38,
5	77,000*	0.223	5	0.1	standard deviation = 1.27)
6	77,000*	0.223	10	0.2	
7	77,000*	0.223	15	0.3	
8	100,000**	0.291	5	0.1	
9	100,000**	0.291	10	0.2	
10	100,000**	0.291	15	0.3	

## Table 7-1 Scenarios used for WQOA

\*Estimate for ca. 2040. \*\* Estimate for ca. beyond 2060.







Figure 7-1 WQOA locations





## 7.2 Water quality data review outcomes

Prior assessments conducted that looked at the impacts of the existing STP on Molonglo River and LBG water quality concluded that the release of fully treated sewage effluent to the river can have both positive and negative impacts on the receiving environments. The impacts are summarised as follows:

### 7.2.1 **Positive impacts**

- Effluent discharge from the STP contributes to baseflow and is considered a positive impact on the Molonglo River and downstream, including providing flows to LBG. Since the construction of the Googong Dam, the STP is one the few sources of inflow into the lake in very low flow conditions
- The STP discharge contains nitrogen in the form of nitrate. When nitrate from other sources are lacking, nitrate entering the lake offsets potential adverse conditions occurring in waters at the bottom of the lake.

#### 7.2.2 Negative impacts

- The loading of phosphorus and BOD in the effluent discharge can contribute to blue-green algae growth.
- STP operations can be affected by heavy rains or flood events. For these events, a series of by-passes are
  designed to protect the sewage process systems. The by-pass directs partially treated sewage to a series of
  maturation lagoons where it is mixed with fully treated effluent prior to discharge. Under extreme flood
  conditions, faecal bacteria can be washed out from the maturation lagoon system. It is also worth mentioning
  that while spills of untreated sewage contribute to faecal contamination that can potentially lead to lake closures,
  such events are infrequent. The long-term contaminant loads from the STP under by-pass conditions is likely to
  be quite minor compared to the large loads of faecal bacteria entering the catchment system from other sources
  (e.g. overland runoff from urban/industrial areas, domestic animals and grazing areas, etc.).

Water quality data was collated from the ACT Government, Icon Water and QPRC with an aim to further test the outcomes from water quality modelling and ascertain the STP impact. However, the nature of available river water quality data collected upstream and downstream of the Queanbeyan STP did not enable clear conclusions to be drawn about the impact of the STP on the Molonglo River, especially during STP diversion events. Upstream of the STP the urban and agricultural land-use influence river water quality, especially total nitrogen and faecal coliform concentrations. Downstream of the STP there is a greater percentage of total nitrogen and chlorophyll-a concentrations that are above relevant guideline concentrations, which may be influenced by STP inputs, but also by other land-uses in the vicinity of the downstream water quality site on the Molonglo River. During STP diversion events the small amount of matching river water quality data does indicate that there are increased faecal coliform concentrations of the effluent. However, there is a lack of before, during and after diversion river water quality data to draw conclusions of the effects of STP diversions on river water quality. Historically, diversion events from the STP have been associated with elevated faecal coliform concentrations in the Molonglo River, but there is a lack of data to empirically understand broader water quality responses during and immediately following these events.





## 7.3 Water quality modelling approach

The data analysis highlighted that suspended solids, dissolved oxygen and pH levels in the Molonglo River downstream of the STP are generally within recommended guideline levels under the STP's current operation. The suspended solids levels of the effluent have generally been more favourable than the background water quality in the Molonglo River, suggesting that the existing licencing conditions (and indeed STP performance) is providing adequately for managing solids content.

A prior review has identified that the biological oxygen demand (BOD) may be having negative impacts in terms of algae growth potential in the lake; however no BOD data was available for the effluent and the dissolved oxygen levels in the river downstream of the STP tend to be within guideline values. Guideline exceedances were mainly associated with nutrient and coliform levels in the Molonglo River. Understanding the nutrient and faecal coliform impacts of the effluent on the receiving waters, and the complex impacts of future increases in the serviced population and discharge rates, required further investigation.

Detailed models of the Molonglo River quality in the reach from the present STP to LBG were developed. The model was then used to understand the 'baseline' water quality of the river in the hypothetical absence of any STP discharging into the river. This baseline was superimposed with several test scenarios for various future STP loading, effluent quality and flow rate permutations to understand the impacts that future plant operations may have on receiving water quality.

## 7.4 Water quality model findings

The models suggest that in the vicinity of where the Molonglo River enters the LBG (even under future possible plant arrangements and EPs):

- Total nitrogen (TN) levels in the river can perhaps be managed to levels similar to the present and historical case even allowing for an increase in served population by adopting an effluent target in the range 5 10 mg/L. Presently the STP achieves effluent TN with a mean of 16 mg/L and 90th percentile of 26 mg/L.
- If total phosphorous (TP) effluent targets of 0.1 0.2 mg/L were adopted there would be insignificant to minor increases on TP content of the Molonglo River due to the influence of background levels of TP just upstream of the STP and other inputs downstream such as the turf farm, and the river and water quality processes. Note also that the present plant already achieves effluent average TP levels of 0.09 mg/L and 90th percentile of 0.15 mg/L
- The STP effluent is likely having little impact on the presence of coliforms at this site, owing to the relatively lengthy travel and residence times and the processes of microbiological decay. The scenario 1 (no STP) model results are very similar to those outputs for all other scenarios, indicating coliform sources closer to the location (i.e. other than the STP) are likely to be much more influential. Achieving similar or greater levels of log-reduction of coliforms at the STP in future may not translate into observable improvements in coliform presence at this site. Again, note that the historical median faecal coliform measurement in the STP effluent is 28 cfu/100mL, while the median measured in the river just upstream of the STP has been 170 cfu/100mL, suggesting that outside of acute impacts of wet weather bypass event periods, the STP discharge is beneficial to the balance of faecal coliforms in the river.

By extension adopting the targets for effluent quality in the ranges listed above would suggest that there would not be significant increases in nutrient or coliform concentrations in the river water entering LBG, even allowing for future load increase. However, if concentrations are maintained then the greater flows from the future plant could increase the overall loads of nutrients entering the lake, which is important particularly from the perspective of algal bloom potential. This is illustrated by Figure 7-2 and Figure 7-3.

















## 7.5 Setting effluent quality objectives

The modelling outcomes indicate that, with regard to the nutrient river quality at the confluence with Lake Burley Griffin, a 'negligible or beneficial impact' outcome on water quality concentrations may be achieved by adopting effluent quality targets of 5-10 mg/L for TN and 0.1-0.2 mg/L for TP. These could be suitable as target median and 90th percentile effluent concentrations respectively. The present licenced faecal coliform effluent objectives and performance has served adequately to provide a beneficial impact on measurable coliform concentrations in the Molonglo River. As such, the historical performance of the effluent could be adopted as formal future targets for coliform presence in the effluent which would correspond to median of ca. 30 cfu/100 mL and 90th percentile of ca. 200 cfu/100 mL. These values correspond to some of the more stringent licence conditions at other STPs in New South Wales. Such values would improve the presence of pathogenic organisms in the effluent and hence the receiving environments. Future rationale for alternate coliform (or other microbial) level indicator may be dictated by a desire to treat water to levels appropriate for beneficial reuses by achieving log-reduction targets outlined in the Australian Guidelines for Water Recycling (2006).

The present BOD and suspended/dissolved solids licencing conditions can be considered as starting points for discussions about future licencing conditions, noting that the receiving water quality impacts are within current guideline limits.

## 7.6 ACT EPA licence requirements

As indicated in section 4.3.10, a new licence would be required for an upgraded STP. This licence would be set to meet the requirements of the *Environmental Protection Regulations (2005)*, Schedule 4, Part 4.7. These requirements have therefore been taken into consideration in the basis of design outcomes.

## 7.7 STP bypass event modelling

Operation of the Queanbeyan STP can be affected by heavy rains or flood events. For these events, a series of bypasses are designed to protect the sewage treatment process systems. The by-pass directs partially treated sewage to a series of maturation ponds where it is mixed with fully treated effluent prior to discharge. Extreme flood conditions can result in this water being washed out of the maturation pond system and into the Molonglo River, potentially resulting in rapid declines in water quality.

The potential impact of the STP bypass events on the water quality within the Molonglo River was assessed using the MIKE11 ecological processes model previously developed as part of the Queanbeyan Sewage Treatment Plant Objectives Review and Assessment prepared by AECOM (2015) for QPRC. This model extends from the confluence of the Molonglo and Queanbeyan River upstream of the STP down to Lake Burley Griffin, and simulates variations in Total Nitrogen (TN), Total phosphorus (TP) and Faecal Coliforms. For details on the model development and calibration refer to the above mentioned report.

The available data on STP operation during normal conditions and during bypassing events were used to develop a number of model simulations to cover a range of possible bypassing scenarios. A total of 18 events were derived based on 3 actual bypass events occurring during the second half of 2010. These events were selected as they provide a good representation of the range of bypass flow volumes and durations that can occur.

As expected, the shorter duration bypass events with higher nutrient and faecal coliform concentrations resulted in a plume with significantly higher concentrations than the longer duration bypass events with lower concentrations of nutrients and faecal coliforms.

The long term modelling undertaken for the Queanbeyan STP Objectives Review and Assessment found that the plume from the STP generally took in the order of a month to reach the Dairy Flat Road water quality monitoring site. The increased flow in the Molonglo River during bypass events acts to dilute the plume from the STP. The amount of dilution is dependent of the magnitude of the Molonglo River flows relative to the STP bypassing flows.

For STP bypassing occurring during more regional scale flood events where there are large concurrent flows within the Molonglo River the impact of STP bypassing is small, even for longer durations of STP bypassing with high





nutrient and faecal coliform concentration. The December 2010 bypass event is representative of such a case, where there is minimal change in the water quality in the Molonglo River.

## 7.8 Concluding observations

The following effluent discharge criteria shown in Table 7-2 are considered appropriate and unlikely to result in a net increase of impacts on downstream water quality. The design outcome should also be based on 100% river discharge.

Parameter	Units	Performance	Statistic	Proposed Licence Limit (100%ile)
Total Nitrogen	mg/L	10 5	90%ile 50%ile	10
Total Phosphorus	mg/L	0.15 0.1	90%ile 50%ile	0.2
Faecal coliforms	cfu/100mL	30 200	Median 90%ile	60
BOD	mg/L	10 5	90%ile 50%ile	10
Suspended Solids	mg/L	10 5	90%ile 50%ile	10

#### Table 7-2 WQOA outcomes for performance of STP and proposed licence limits





# 8 Sustainability

## 8.1 General

There are various legislative (State and Federal) and policy requirements that must be fulfilled in order to set up the project and ensure compliance. A key deliverable among these requirements is incorporating Sustainability into the Project Management Framework (PMF) and minimising the environmental and social impact of the resulting STP. A policy framework document has been developed that lists these legislations / policies, which specify sustainable outcomes and their relevance to the STP project.

QCC's "Sustainable Building Design Policy" was adopted in March 2013 to help Council fulfil its legislative obligations, as outlined in the framework document. The Sustainable Building Design Policy required Council Infrastructure projects (with a total expenditure greater than \$3,000,000) obtain External Certification to ensure compliance with Council's Sustainability obligations and facilitate Triple Bottom Line reporting. The STP project falls within this requirement.

Benefits to Council in adopting this level of evaluation include:

- Rigorous assessment of risk management and proficiency of design, construction and operation
- Recognition as a leading public infrastructure project with certified sustainability rating
- Capacity building through knowledge and training of staff in water sensitive urban design, sewerage management and plant design
- A final facility with zero or negligible impact on the environment
- Rewards for excellence in best practice technology with demonstrated level of zero net impact on the environment
- Improved experience and credibility of the project team in sustainability principles
- Prestige and proven ability to create a long-term legacy of a sustainably engineered facility.

Under the policy, Council is obliged to obtain external certification of sustainability outcomes for the STP Project. The PMF incorporates this requirement and the policy was used to select a suitable external certifier. Council has engaged the Infrastructure Sustainability Council of Australia (ISCA) to be the external certifier for the project.

## 8.2 ISCA and the IS rating tool

The IS (Infrastructure Sustainability) rating scheme for infrastructure is developed and administered by ISCA.

ISCA's measurement tool, the IS Rating Scheme, has been designed to measure a range of sustainability criteria across design, construction and operation, with some of the major themes comprising:

- Management and governance
- Using resources
- Emissions, pollution and waste
- Ecology
- People and place
- Innovation.

Importantly, the tool is designed to achieve sustainable outcomes without an increase in capital cost, through strategies such as improved decision-making, more effective stakeholder / community consultation, evidence and data collection.





## 8.2.1 IS Rating for the STP

Getting an IS rating for the STP would help QPRC demonstrate compliance with Federal, State and QPRC internal policies. In the instance that Council is able to achieve an IS rating of "Excellent", compliance with the Sustainable Building Policy would be achieved as described below.

The major target for Council's "Sustainable Building Design Policy" is a "Zero net impact on greenhouse gas and water use compared to previous years" for the "As Built" product leading to:

- No Net increase in Green House Gas Emissions
- No Net increase in Council Water Use
- Increase waste recovery rates to 80%.

There are three ratings that can be awarded to infrastructure projects that go beyond business as usual:

- · Commended (Measurement and Implementing Initiatives)
- Excellent (No Net Impact)
- Leading (Restoration and Enhancement).

The ratings can be achieved for the following stages:

- Design
- As Built
- Operation.

However, baseline data informing the current performance of Council's STP against the above mentioned factors is required to provide a benchmark against which the performance of the new STP will be measured. In order to achieve this, an "Operational" Rating for the existing STP will be sought. For the new STP, QPRC will seek a "Design" leading to an "As Built" rating.

Council's Sustainability Officer is responsible for managing the external certification process for the Project with support by a suitably qualified and experienced consultant.

#### 8.2.2 Future Projects

In compliance with the Sustainable Building Policy, QPRC will need to get external certification for any projects with a total expenditure in excess of \$2,000,000. Future projects like the CBD Upgrade and the Ellerton Drive connection would fall under this category. The experiences gained from using ISCA for the STP would be transferrable to other projects leading to a more streamlined approach to sustainability certification for future projects. This capacity building for QPRC staff will facilitate better sustainability outcomes for future projects without (completely) relying on support from external consultants.

#### 8.3 Reuse of Effluent

Currently, QPRC does not reuse treated effluent from the Queanbeyan STP as no suitable reuse options have been identified. There is the potential that reuse options may be identified in the future. As such, it is recommended that a recycled water study be undertaken that can identify reuse options for future development stages of Queanbeyan STP. This may assist QPRC in managing any new environmental licence conditions imposed on the future STP, as well as meeting the expectations of stakeholders in committing to nutrient reduction in the downstream river and lake.

## 8.4 Concluding Observations

The project delivery should consider sustainability in all project related activities (including project management, procurement, materials selection etc.) with the goal of obtaining Design and As-Built IS ratings of Excellent with an IS score in the range of 65 to 75% or better.

Undertake a recycled water study to determine the viability of reuse in the future which also considers potential impacts on the yield of the Molonglo River and downstream users.




## 9 Treatment technology approaches

Various technology options were considered for each step in the treatment process as a preliminary starting point, notwithstanding the Concept Design stage. These are included in this Masterplan Report for completeness. The selection of the treatment process train will be determined during the concept Design phase of the project. All options reviewed are detailed in Appendix G.

## 9.1 **Preliminary**

#### 9.1.1 Screening

- Coarse Simple bar racks spaced 1-10 cm apart to remove large debris. Wire or bar screens are spaced 6-10 mm apart for finer screening
- Fine Smaller apertures, range of 1-6 mm. This is often used to protect downstream processes such as membranes
- Mechanical Belt Sieve has the potential to reduce the suspended solids load on the treatment plant by 30%

#### 9.1.2 Grit Removal

- Horizontal Flow flow velocity is controlled in a long, narrow basin. Permits heavier grit to settle
- Aerated Spiral flow pattern is induced in a grit chamber. Acceleration causes heavier grit to settle. Also strips odorous compounds
- Vortex system uses gravity and centrifugal forces to separate grit and sweep it into a collection chamber.

## 9.2 Primary

#### 9.2.1 Equalisation tanks

Wastewater flow rates and loading rates vary greatly depending on day, week or season. Equalisation tanks are sometimes used to buffer influent flow and load which benefits biological treatment.

#### 9.2.2 Primary Settling

Velocity of wastewater is greatly reduced to remove organic solids that will readily settle. Primary settling can remove 50-60% of suspended solids and 25-35% of BOD<sub>5</sub>.

## 9.3 Secondary

#### 9.3.1 Suspended growth processes

The activated sludge process utilises an aeration tank where aerobic bacterial culture is maintained in suspension:

- Activated Sludge with Biological Nitrogen Removal (BNR):
  - The first and simplest BNR plant was the Ludzak-Ettinger process, which incorporates an anoxic zone and relies on the nitrate formed in the aerobic zone being returned via RAS to the anoxic zone to undergo denitrification
  - The modified Ludzak-Ettinger process involves the addition of an internal recycle to feed more nitrate to the anoxic zone. The Bardenpho process incorporates a second anoxic zone post aerobic zone, allowing further denitrification to occur





- Activated Sludge with Biological Nitrogen and Phosphorous Removal:
  - 3-Stage Phoredox: A modification of the MLE process incorporating an anaerobic zone for phosphorus removal. The 5-Stage Phoredox process incorporates an anaerobic zone for phosphorus removal prior to the first anoxic zone, and secondary anoxic and re-aeration zones for improved nitrogen reduction
  - UCT configuration: Designed to largely eliminate the effect of nitrate in the upfront anaerobic zone, as when nitrate is present, bacteria will use this nitrate and consume organics, leaving less organics available for phosphate-accumulating organisms.
- *Pasveer Oxidation Ditch:* A continuous flow, activated sludge system where wastewater is mechanically circulated through a ditch with rotors that agitate and aerate the influent. The aerated wastewater is allowed to settle and the activated sludge is removed. A portion of the sludge is returned to the ditch in order to promote microbial activity.
- Sequencing Batch Reactors: An activated sludge process designed to operate in batch or non-steady state conditions. The SBR tank carries out the functions of equalisation, aeration and sedimentation in a time sequence rather than in the conventional space sequence of continuous-flow systems.
- Aerobic Granular Sludge: Consists of aggregates of microbes that coagulate and settle significantly faster than typical activated sludge flocs. The high sludge settling rates achieved with granular sludge, result in smaller reactor volumes and a short-duration settling phase.
- *Membrane Bioreactors:* Combines activated sludge treatment with a membrane liquid-solid separation process. The membrane component uses low pressure microfiltration or ultrafiltration membranes and eliminates the need for clarification and tertiary filtration.
- *Facultative Lagoons:* Do not provide biological nutrient removal, however they can provide a satisfactory level of treatment where wastewater is disposed to land, depending on discharge requirements. Lagoon systems provide primary sedimentation as well as a significant equalisation effect, and can also provide biological treatment.

#### 9.3.2 Attached growth processes

Attached growth processes remove soluble and colloidal organic materials by the means of a biological film on a fixed media. This film typically comprises a large and diverse population of organisms:

- *Trickling Filters:* Consists of a shallow bed filled with crushed stones or synthetic materials. Wastewater is introduced over the bed and a biofilm is created that becomes thick and falls off (sloughing). The popularity of trickling filters has declined with increasing requirements for biological nutrient removal.
- *Moving Bed Biofilm Reactor:* Utilises specialised plastic carriers to create a surface on which a biofilm can attach. The waste water enters the first Moving Bed Biofilm Reactor at low level and over flows via screened ports at high level until it passes with unattached biomass into the clarifier.
- Integrated Fixed Film Activated Sludge: Incorporates an attached growth media within a suspended growth reactor. As such, the Integrated Fixed Film Activated Sludge still requires a large activated sludge clarifier and sludge return system.





## 9.3.3 Anaerobic processes

Anaerobic processes are mostly used in the treatment of high strength industrial wastes. For domestic wastewater applications, the most widely used anaerobic processes are septic tanks, anaerobic lagoons, and the Upflow Anaerobic Sludge Blanket (UASB):

- UASB: Influent wastewater is distributed at the bottom of the reactor and migrates upwards through a sludge blanket. The organic components in the wastewater are converted into biogas which is collected in the gas solids separator at the top of the UASB reactor.
- Anaerobic Lagoons: Deep earthen basins with sufficient volume to permit sedimentation of settleable solids, to digest retained sludge, and to anaerobically reduce some of the soluble organic contaminants. Raw wastewater enters near the bottom of the pond and mixes with the active microbial mass in the sludge blanket.

## 9.4 Tertiary

#### 9.4.1 Filtration

- Depth Filtration Uses a porous median (such as sand) to retain particles throughout the media
- Surface Filtration Involves removal of particulate material by mechanical sieving. Filter pore sizes range from 5-30 μm
- Membrane Filtration Involves use of membranes with very small pore sizes in the range of 0.01-1 μm.
   Processes used are:
  - Microfiltration 0.07-2.0 μm
  - Ultrafiltration 0.008-0.2 µm
  - Nanofiltration and Reverse Osmosis <2 nm high pressure process. Also uses electro dialysis.

### 9.4.2 Adsorption

Adsorption is used to remove substances such as nitrogen, sulphides and heavy metals by accumulating the substances in a solid medium. The most common solid adsorbent is activated carbon.

## 9.5 Disinfection

Disinfection is the primary mechanism for inactivation/destruction of pathogenic organisms.

#### 9.5.1 Chlorination

The most commonly used disinfectant technique. Several chlorine compounds include:

- Chlorine: Used as a gas or pressurised liquid. Highly toxic
- Sodium Hypochlorite: Aqueous solution with around 12-17% chlorine. Less hazardous than chlorine but more expensive
- Calcium Hypochlorite: Dry form, meaning easier transport and storage. Dissolution required before dosing difficult in large installations
- *De-chlorination*: May be required before discharge of effluent to the environment, due to toxicity of residual chlorine.

#### 9.5.2 Ultraviolet

UV radiation damages microorganisms and interferes with the processes of cell synthesis and cell division.





## 9.5.3 Ozone

Ozone is an extremely reactive oxidant that disinfects as a result of cell wall disintegration. Generally used at medium-large sized plants. Also helps with odour control.

## 9.6 Sludge handling

### 9.6.1 Thickening

Concentrates sludge solids and reduces its volume. Generally accomplished through physical processes such as:

- Gravity Thickening: Undertaken in circular tanks similar to primary and secondary settling tanks.
- *Dissolved Air Flotation*: Achieved by dissolving air in wastewater then releasing into a flotation tank at atmospheric pressure
- *Centrifuge*: Sludge is fed to a rotating bowl that contains an accelerating inlet rotor, creating centrifugal forces that push solids to the outer wall. Used at medium to large plants
- *Gravity Belt Thickener*. Consists of conditioning and polymer system and rotating cylindrical screens. Conditioned sludge is fed to the rotating screens which separate the flocculated solids.

#### 9.6.2 Stabilisation

Undertaken to reduce pathogens, eliminate offensive odours and reduce or eliminate the potential for further degradation of organic matter. Stabilisation can be undertaken through biological, chemical or physical means. The main methods of stabilisation are:

- Alkaline Stabilisation: The addition of alkaline material maintains a high pH level and causes the destruction of pathogenic organisms
- *Anaerobic Digestion*: Involves the decomposition of organic matter with no oxygen present. Anaerobic microorganisms consume organic matter and produce methane and carbon dioxide
- Aerobic Digestion: Involves aeration of sludge, similar to activated sludge. Commonly used at smaller plants and those without primary settling and sludge, for stabilisation.

#### 9.6.3 Conditioning

Sludge and biosolids are conditioned in order to improve their dewatering characteristics. The most common conditioning agents are polymers, used to achieve flocculation or aggregation of solids and therefore achieve efficient solid-liquid separation.

#### 9.6.4 Dewatering

Dewatering is undertaken to remove water and produce a high solids content final product called biosolids cake. Dewatering techniques are mostly mechanical.

- *Centrifuge*: Commonly used for dewatering wastewater biosolids. Sludge is fed to a rotating bowl that contains an accelerating inlet rotor creating centrifugal forces that push solids to the outer wall of the bowl
- *Belt Filter Press*: Sludge is firstly conditioned with polymer and then distributed evenly over the width of the belt. The belt filter press applies mechanical pressure to force the separation of water from the sludge
- *Plate Filter Press*: The plate filter press is comprised of a series of filter chambers formed between filter plate presses supported on a metal frame. The plates are clamped together with hydraulic rams, and the high pressure gradually dewaters the sludge
- Rotary Fan Press conditioned sludge is fed into the enclosed slow moving (<1 rpm) dewatering channel between two parallel stainless steel, filter screen plates





- *Screw Press*: Flocculated sludge is pumped into a cylindrical screen basket wherein an auger slowly rotates. The diameter of the auger's shaft increases towards the end of the basket and the gap between its flights decreases. This change in volume causes a change in pressure that dewaters the sludge
- *Solar Dryers*: Sludge is loaded into a drying hall and is slowly turned from one end to the other. Water evaporates, leaving 65-80% DS.

## 9.7 Ancillary processes

### 9.7.1 Chemical Dosing

Chemical dosing is undertaken in a variety of circumstances at STPs and can be employed in a solid, liquid or gaseous form. Chemical dosing systems are generally designed to be either batch or constant feed.

#### 9.7.2 Odour Control

Odours at treatment plants can be minimised by proper attention to design details, such as the use of submerged inlets and weirs, minimising turbulent areas, proper process loading rates, covering or containment of odour sources, and off-gas treatment.

- Activated Carbon: Adsorption through beds of activated carbon is a commonly used odour treatment method.
- *Bio-tricking Filters*: A biofilm layer of microorganisms supported by packed bed filters absorb and oxidise odorous gases.
- Chemical Scrubbers: Allow oxidation of odorous compounds through contact with air, water and chemicals.





## 10 Solids management

## 10.1 Introduction

QPRC will need to consider management of the biosolids that are produced as by-products of the wastewater treatment process from the STP. Solids management strategies implemented by other local councils and utilities were reviewed and compared to identify options suitable for implementation at Queanbeyan STP.

This section summarises the findings of investigations into solids management options, notwithstanding the Concept Design stage. For further detail, refer to Appendix F.

## 10.2 Local regional solution

Several councils and utilities around the local region were contacted to gain an understanding of their solids management procedures, capabilities and future plans. The informal discussions were focused around answering the following high-level questions:

- What are the current procedures being adopted for your solids management?
- Would your council/group have capacity for accepting the solids that are produced from Queanbeyan STP?
- Would your council/group consider giving their solids to QPRC as part of a larger regional solution?

The responses from various councils and groups are summarised below:

- *LMWQCC (ACT):* Currently all streams of solids arriving at LMWQCC enter by sewer. The sewage is treated and the solids are removed before being incinerated in a furnace. It may be feasible for LMWQCC to receive more waste; however the EPA licence restricts the furnace from receiving solids from other sources. Incineration of the solids produces a soil-enhancing product called Agri-Ash, which is sold for agricultural use. By giving solids to another facility LMWQCC would generate less income from Agri-Ash.
- Mugga Lane Resource Management Centre (MLRMC): ACT NOWaste's MLRMC is the only putrescible waste landfill in the ACT. MLRMC currently disposes of approximately 290,000 t/y and is undertaking capital works to increase the capacity. Currently there are no solids from sewage treatment being received by MLRMC, but NOWaste have advised that there would be no issues with doing so. They would also likely consider giving organic solids to another facility as a collaborative solution for resource recovery.
- Murrumbateman Landfill (NSW): This is the only licensed landfill operated by Yass Valley Council. The landfill
  is licensed under EPA for application of waste to land, including non-putrescible biosolids and dewatered
  putrescible grit or screenings from sewage treatment systems. This landfill is being converted into transfer
  stations, and waste will ultimately be disposed of at the regional landfill facility at Bald Hills near Jugiong.
- Yass STP (NSW): The Yass STP is capable of treating sewage for 6,800 EP and has allowed for future expansion to 10,800 EP. Currently grit and screenings are bagged and disposed of on site. There is storage space for several more years, but when full the waste will be trucked to the regional landfill facility in Bald Hills. Council is considering the options for someone to take sludge waste, potentially to be used as a land fertiliser. Under EPA licence Yass STP may receive and process products from other STPs.
- New Murrumbateman STP (NSW): Yass Valley Council has recently completed a new STP at Murrumbateman. It is expected that sludge generation from this treatment plant will be small initially and not require disposal for several years. Council would prefer a solution which is close by for giving away their sludge. However, if there were no nearby solutions found, the Council would likely consider giving sludge to a regional facility with QPRC. The cost of transportation of the sludge waste to the Queanbeyan region would likely be a major factor for Council.





- *Palerang Landfill Sites (NSW):* The former Palerang Council (now amalgamated to QPRC) has several landfill sites in the region. These landfills are progressively being closed and all waste will ultimately be transferred to the Woodlawn Waste and Resource Management site located within the Goulburn Mulwaree Council area.
- *Braidwood STP (NSW):* There are currently three STPs within the former Palerang Council area; at Captains Flat, Bungendore and Braidwood. The grit and screenings from the three STPs are all disposed of at landfill sites. Palerang Council advised they would be open to discussion about the option of giving sludge from STPs to a regional solution with QCC.
- Landtasia Organic Farms (NSW): Currently the Landtasia Organic Farms site in the former Palerang Council
  receives food and garden waste from the local region for composting and producing a solution for agricultural
  soils. Acceptance of biosolids is not part of the current Environmental Protection Licence (EPL) at Landtasia. It
  is unlikely that the licence for the existing site would be able to be upgraded to receive biosolids, due to its
  locality within the Sydney Catchment Authority region. While Landtasia is not able to accept biosolids, the
  operators at Landtasia are well experienced to assist the QPRC in developing (or operating) their own
  composting facility which accepts biosolids.
- Glen Wastewater Treatment Facility (NSW): Around 200-250 kg/d of grit and screenings is produced and taken by garbage truck to Cooma Landfill Resource and Waste Facility. A further 400 – 500 t/y of sludge is produced at the STP which is discharged into one of two sludge lagoons for drying. The sludge lagoons each have a capacity of around one year's volume of sludge. Every two years, after both sludge lagoons have been filled, the sludge is dewatered through a centrifuge (by an outside contractor) and carted to the Cooma landfill site. Cooma Monaro Shire Council would likely be interested in the option of giving sludge to a regional solution with QPRC, particularly since the disposal of sludge to Cooma landfill comes at a cost.
- Goulburn Mulwaree Council (NSW): There are currently two STPs in the Goulburn Mulwaree Council area; Goulburn STP and Marulan STP. Currently the STP solids are disposed of at a local farm in accordance with a licence under the NSW EPA. A new Goulburn STP is due for completion mid-2017. With the new STP upgrade, Council will be looking for additional solids disposal options. They are open to giving their solid waste to QPRC and would appreciate having discussions regarding any collaborative solutions.
- Woodlawn Waste and Resource Management Site (NSW): The Woodlawn Bioreactor currently receives 20% of Sydney's putrescible waste which is used to generate green electricity. Currently the site contains around 4 million tonnes of waste. The bioreactor would likely have capacity for receiving the solids from QPRC STP, however the solids would need to be in a suitably dry form to comply with the current licence.
- Holcim Quarry (NSW): Holcim have expressed interest in a proposal that involves remediation of the land on their site using a mix of biosolids and VENM (Virgin Excavated Native Material). QPRC currently has stockpiles of biosolids and green waste that could be mixed with VENM from Googong to create a commercially viable product.

## 10.3 Agricultural land application

## 10.3.1 Fertiliser / Soil conditioner for human crops production

Enhancing crop production by using sewage waste on land is a longstanding practice. In the past, farmers depended solely on various organic products and wastes until chemical fertilisers were invented to enhance crop production. This option is already being used extensively in Canberra with the quality product being received from Sydney. Environmentally this is a sound option and there is plenty of human crop productions close enough to the Queanbeyan STP to make the option worthwhile. Profitability of the option due to the cheap market rates is an issue. Increased funding or grants from the NSW Regional Regulated Area (RRA) or the Environment Protection Authority (EPA) even though it won't provide renewable energy to the plant seems a feasible option. There is also benefit of partnerships with Canberra Investment Corporation Limited and Googong Township Pty Ltd.





## 10.3.2 Fertiliser for animal crops production

Biosolids contain a range of valuable nutrients such as nitrogen, phosphorus, iron, calcium, magnesium and various other macro and micro nutrients which are essential for plant growth. Many of these nutrients are also essential components in the healthy diet of animals in order to maintain growth and for food production. There have been successful grazing experiments in Goulburn NSW, showing that application of dewatered biosolids significantly increased pasture production and livestock performance.

The use of biosolids as fertiliser for animal crops production has fewer problems with odour than other alternatives and the crops are in rural areas making limited opportunity for community complaints. As this can be seen as a way to help the farmers and agricultural industry, grants or increases in funding are likely as there is an industry in Queanbeyan for agriculture.

## **10.4** Non-agricultural land application

#### 10.4.1 Forestry

Land application of biosolids within forests is a relatively new practice. This use had been difficult to achieve due to technology limitations in spreading biosolids evenly through heavily forested areas. However, various residuals, including pulp and paper mill sludge, ash, industrial residues, sewage sludge and wastewater, are utilised to enhance growth of forest ecosystems.

Environmentally this is a very good option and there is forestry close enough to the Queanbeyan STP to make the option economically viable.

The main concern would be the cost of transporting and spreading the biosolids. As there is a likelihood of receiving increased funding or grants this option appears feasible. A service provider would need to be identified.

#### 10.4.2 Land reclamation

Biosolids have several characteristics that make them suitable for reclaiming and improving disturbed and marginal soils. The organic matter in biosolids improves the soil physical properties by improving granulation, reducing plasticity and cohesion, and increasing water-holding capacity. Biosolids increase soil cation exchange capacity, supply plant nutrients and buffer soil.

The opportunity of land remediation at the Holcim Quarry makes this option very feasible. This would provide a long term solution for biosolids management. The cost of transporting the biosolids is low and the likelihood of receiving increased funding or grants for this option is high, with the EPA ready to help businesses divert waste from landfill.

#### 10.4.3 Mine site reclamation

The most widespread use of biosolids for land reclamation is repairing land damaged by mining. The restoration of mine soils with biosolids has been shown to increase soil organic matter, cation exchange capacity, soil nutrient levels, and to promote soil ecosystem recovery.

However, this is not an acceptable option as there are no mine reclamation sites in the proximity of the QPRC LGA; the nearest mine is at Thuddungra (200 km away).

#### 10.4.4 Horticulture and landscaping

The use of biosolids for horticulture and landscaping is similar to land and agricultural application, but with a different intent. The biosolids product, often compost, is used for soil conditioning rather than as a replacement fertiliser. This is a viable option as there is a golf club, five nurseries and 14 football/cricket grounds located in Queanbeyan, all of which could make use of biosolids for landscaping purposes (soil conditioning).

The costs for transport will be low as the STP is in close proximity to the golf course and the football / cricket grounds. The likelihood of receiving increased funding or grants for this option is highly likely due to the existing use in Australia. As such, use for horticulture and landscaping in the QPRC region could be cost effective and feasible.





## 10.5 Energy recovery – Renewable energy resources

### 10.5.1 Thermal energy recovery – Heat generation

Utilisation of unused energy such as industrial waste heat is an important measure for reducing energy consumption to mitigate global warming and reduce heat waste. Recovered thermal energy may be utilised at the new treatment plant in a similar manner to LMWQCC to warm the raw sewage influent, or (with the aid of co-generation) used to provide power for the treatment plant. Although this option could enhance sustainability, it would do so at a higher initial capital cost compared to using natural gas.

#### 10.5.2 Fuel production – Oil from sludge process

Conversion of sludge, which is heavily contaminated by heavy metals and/or toxic chemicals to oil is technically feasible, however capital and running costs of such processes are high. The Queanbeyan STP will not produce near enough sludge to make this solution economically viable.

#### 10.5.3 Energy recovery – Gasification

Co-incineration with municipal solid waste has been effectively used elsewhere. However, this isn't a feasible solution for the Queanbeyan STP as a gasification plant requires a power plant close by which is not the case for the STP.

## 10.6 Other uses

## **10.6.1** Recycling and use as a construction material

Recycling sludge for use as a construction material is becoming increasingly popular as it can be readily applied as well as the economic and environmental advantages. Given the close proximity of many construction suppliers this appears to be a good solution to the high demand for recycled sludge materials. Environmentally this solution is better than similar alternatives due to the use of construction material with lower embedded energy. Although the cost of recycling sludge to create construction materials is relatively high the option could become economically viable depending on the demand for such materials.

#### 10.6.2 Commercial uses of biosolids

Efforts to "market" biosolids generally refer to the sale of large quantities to commercial consumers. Biosolids may also be sold in smaller quantities to homeowners and gardeners. In the first instance the new Queanbeyan STP is unlikely to be large enough to be commercially viable but may become so in the future.

## 10.7 Comparison

Comparing the potential solutions for biosolids disposal indicates that two solutions are not viable due to the location of the new STP in relation to potential users of the biosolids by-products. To be economically viable, Mine Site Reclamation possible users need to be within 100 kilometres of the new Queanbeyan STP. However, the nearest mine is 200 kilometres away.

The use of biosolids for land reclamation at the Holcim Quarry is seen as the optimal solution as this would provide a long-term, sustainable, and financially viable solution for biosolids management.

Use of biosolids by-product for animal crop production is politically and socially acceptable as the product's safety has been proven in NSW and overseas, there are no odour problems to residents, and animal crop production is a large industry in Queanbeyan. Energy recovery is also an excellent solution due to the increased capacity to move towards energy neutrality for the new STP. This however would need a regional approach to be viable.





Table 10-1	Solids management solution comparison (criteria scores shown are out of 10)
------------	---

Solution	GO NO GO	Sustainability	Local Regional Solution	Cost / Profitability	Politics	Feasibility	Total Score (/50)
Human Crop Production	GO	7	9	8	7	8	39
Animal Crop Production	GO	9	9	7	9	8	42
Forestry	GO	9	7	5	7	7	35
Land Reclamation	GO	9	10	8	8	9	44
Mine Site Reclamation	NO GO	-	-	-	-	-	0
Horticulture and Landscaping (Composting)	GO	9	8	7	7	8	39
Thermal Energy Recovery	GO	9	9	3	6	6	33
Fuel Production	NO GO	-	-	-	-	-	0
Cement Production	NO GO	-	-	-	-	-	0
Gasification	NO GO	-	-	-	-	-	0
Use as a Construction Material (Recycling)	GO	8	6	6	7	6	33
Commercial Use	NO GO	-	-	-	-	-	

## **10.8 Concluding observations**

The solids management solution comparison showed that the most beneficial and viable options were:

- Reuse for land reclamation (e.g. Holcim Quarry Site)
- Production of fertiliser for animal crops
- Production of fertiliser for human crops
- Use for horticulture and landscaping.

These options should be given further consideration during concept design.





## 11 Options Road Map

A Masterplan options workshop was held on 27 November 2014 to discuss and eliminate, where possible, options for the Queanbeyan STP. Attendees at the workshop included the Project Management Team, senior managers from other QCC business units and STP operators. The purpose of the workshop was to determine constraints and identify issues for inclusion in the masterplan to be considered during concept and detailed design. The expected outcome of this workshop was to set the framework for future phases of this project, in particular potential treatment technologies.

The Workshop covered the topics of:

- Where to build?
- What to build?
- Eliminate options?
- What is to be taken forward?

## 11.1 STP location and staging

The existing site is already zoned for sewage treatment and has available space, likely to be adequate for construction of a new STP. Gradual forecasted growth in the Queanbeyan LGA is oriented towards the middle – south of the LGA (as discussed in Section 3). This growth was taken into account and the following points were raised in relation to STP location and staging options.

- Limited use for irrigation on sports fields
- Present infiltration occurring near the racecourse
- No alternate north site exists that may be suitable for a treatment plant
- · Community engagement will have to occur from the start of the project
- · Stormwater ingress to sewers will need to be fixed as soon as possible
- Remedial works are needed for the Morriset Street pump station
- Sewer mining is a possibility at Bayside and Morriset Street pump station.

Considering the above, staging options for the proposed STP to service the LGA were identified and assessed. The outcomes of the assessment were discussed and refined at a stakeholder masterplanning workshop. In particular, the overall deliberation showed that:

- The first stage of the upgrade should be located on the existing STP site and be sized to cater for at least 60,000 EP
- Consequent upgrade stages could either be located at the existing site or be located closer to future growth centres to create a decentralised service
- The timing and extent of the first stage of the upgrade gave considerable flexibility and opportunity to address regional and cross border issues beyond the first stage.

The Road Map for possible options, Figure 11-1, indicates the possible range of upgrade outcomes and the markers that trigger the need for ongoing planning decisions. The associated required infrastructure has been incorporated into the Road Map.

Recycled water is not currently produced at the existing STP and is not being considered for Stage 1 of the STP upgrade. At the Stakeholder Masterplanning Workshop held on 13 February 2015 stakeholders clearly indicated





that recycled water would need to be considered in the future and QPRC agreed to undertake a recycled water study in conjunction with ongoing planning for the STP.



GHD



Figure 11-1 Road map for possible options

Queanbeyan Sewage Treatment Plant Masterplan Last saved; REV 5 / 22 September 2016

Page 66 of 125





CURRENT NEW QSTP NEW PUMP STATION 4KM MAIN REPAIR



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Figure 11-2 Proposed first development

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Figure 11-3 Option 1 between 10 and 25 years

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OPTION 2 Y10-25 BUILD NEW STP AT TRALEE



Figure 11-4 Option 2 between 10 and 25 years

Queanbeyan Sewage Treatment Plant Masterplan Last saved; REV 5 / 22 September 2016







# **OPTION 1A Y25-50** 1 x 100 K EP QSTP



Figure 11-5 Option 1A between 25 and 50 years

Queanbeyan Sewage Treatment Plant Masterplan Last saved; REV 5 / 22 September 2016







OPTION 1B Y25-50 QSTP EXT NEW SSTP



Figure 11-6 Option 1B between 25 and 50 years

Queanbeyan Sewage Treatment Plant Masterplan Last saved; REV 5 / 22 September 2016





OPTION 2A Y25-50 BUILD NEW STP AT SOUTH LGA



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Figure 11-7 Option 2A between 25 and 50 years

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OPTION 2B Y25-50 PUMP FROM SOUTH LGA TO THE ACT



Figure 11-8 Option 2B between 25 and 50 years

Queanbeyan Sewage Treatment Plant Masterplan Last saved; REV 5 / 22 September 2016







OPTION 2C Y25-50 PUMP FROM SOUTH LGA TO TRALEE





Figure 11-9 Option 2C between 25 and 50 years

Queanbeyan Sewage Treatment Plant Masterplan Last saved; REV 5 / 22 September 2016





## 12 Upgrade Options

## 12.1 Introduction and Background

In April 2015, the Office of Water2 (OW) stated some parts of QSTP were possibly reusable. OW requested QPRC to consider three upgrade approaches and propose an approach, which represents value for money3. The OW upgrade approaches included:

- (a) Build a new STP
- (b) Build a new STP, using restored parts of QSTP
- (c) Restore QSTP and expand as needed to provide sufficient capacity.

Technical Memorandum TM004 was prepared for the purpose of assessing the three QSTP upgrade approaches. This is included in Appendix K.

## 12.2 Approach and Method

The QSTP upgrade requires a choice not only of build strategy but also of treatment technology. QPRC intends to deal with technology choices during concept design.

The analysis comprised the following steps:

- (a) Review QSTP condition to identify what (if any) parts of the plant can be readily renewed and used for the new STP
- (b) Identify one or two STP types that could be used to describe the build strategies (options)
- (c) Prepare key criteria for sizing / quantifying the new STP options
- (d) Describe the three build strategies (options) in terms of
  - (i) Treatment process components
    - (ii) Capital and operating costs
    - (iii) Constructability
    - (iv) Operability
    - (v) Sustainability
    - (vi) Future proofing.
- (e) Consider other similar upgrade projects in NSW which might shed light on the decision to either Build New" or "Renew and Augment".
- (f) Undertake a multi-criterion analysis (MCA) to rank options and recommend a build strategy.

## **12.3 Existing STP Condition**

A condition assessment was undertaken, which identified that only the aeration tanks, secondary clarifiers and sludge lagoons could be reused.

The following figure identifies the reuse potential of QSTP.

The inlet works, primary sedimentation tanks, trickling filters and effluent ponds were all discarded as having reuse potential due to their poor condition and in part being affected by the 100 year ARI flood level.

Queanbeyan Sewage Treatment Plant Masterplan

<sup>&</sup>lt;sup>2</sup> The Office of Water in the NSW Department of Planning and Infrastructure

<sup>&</sup>lt;sup>3</sup> Value for Money: A balanced outcome in terms of cost, quality, risk, resource use, fitness for purpose, operability, water quality, environmental protection, and sustainability.







Imagery @2016 CNES / Astrium, DigitalGlobe, Map data @2016 Google

#### Figure 12-1 Reuse Potential of QSTP

## 12.4 Upgrade Options

Six build strategy options were compared. These included consideration of both Conventional Activated Sludge and Membrane Bio Reactor technology for each of the three build strategies. The options were as follows:

Table 12-1	QSTP Upgrade Options
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Option	Build Strategy	Treatment Technology
1A	<b>Build New</b> all process units and equipment, completely abandon the existing plant	BNR - Biological Nutrient Removal CAS - Conventional process
1B	<b>Build New</b> all process units and equipment, completely abandon the existing plant	BNR - Biological Nutrient Removal MBR - Membrane process
2A	Build New main process units and Reuse some process units from STP	BNR - Biological Nutrient Removal CAS - Conventional process
2B	Build New main process units and Reuse some process units from STP	BNR - Biological Nutrient Removal MBR - Membrane process
3A	<b>Renew</b> main QSTP process units & <b>Augment</b> with new additional process units	BNR - Biological Nutrient Removal CAS - Conventional process
3B	<b>Renew</b> main QSTP process units & <b>Augment</b> with new additional process units	BNR - Biological Nutrient Removal MBR - Membrane process





Preliminary site layouts were developed for each option and compared in terms of:

- Constructability
- Operability
- Sustainability
- Future Proofing, and
- Overall Delivery Risk

In addition, to assist consideration of the upgrade approaches, owners of four separate sewage treatment plants that have recently been, or are about to be upgraded were surveyed, and their responses used to inform the option assessment.

The drivers for the plant upgrade appear to have a strong link to the decision to proceed with a new plant, new plant with restored components or restore existing and augment:

- Capacity as a driver is open to retaining parts or restoring the plant for augmentation.
- Stricter licence conditions and in particular the ability to recycle water typically resulted in a decision for a new plant.
- Where capital cost is a primary driver, components may be retained where these perform satisfactorily and are in suitable condition. Items commonly reused are balance tanks, ponds, lagoons and sometimes secondary treatment units.
- Improved biosolids quality did not appear to determine the upgrade approach.
- Asset condition is obviously a key consideration in the decision as to reusing components.

The key drivers for the QSTP are capacity, stricter licence conditions and asset condition of most of the existing STP structures. Based on the lessons learned above, a preference for a new STP (Options 1A, 1B) would be expected.

## 12.5 Cost Estimates

CAPEX cost estimates were prepared for the six options and include construction of new works, rehabilitation of existing structures (where applicable), construction of other supporting capital works, additional preliminaries for extended construction (where applicable), Survey, Investigation and Design (SID) and contingency allowance of 25%. The CAPEX cost estimates fall within a range of plus or minus 5% which is within the level of estimating accuracy, which means that the options cannot be separated on a CAPEX basis. However, it is noted for each option, that the CAPEX cost of the BNR CAS option is slightly more expensive than BNR MBR.

The OPEX cost estimates include labour, power, chemicals, UV lamp and diffuser replacement, membrane replacement (7-year life adopted), Electrical and Instrumentation replacement each 17 years and disposal of biosolids. The OPEX estimate for the BNR MBR options is approximately 15% higher than the BNR CAS options.

The NPV was assessed using a Market Attractive Rate of Return (MARR) of 7%, and tested for sensitivity using rates of 4% and 10 %. The NPV costs fall within plus or minus 2% of each other making the difference between the options again insignificant on a cost basis. The slight advantage of the lower CAPEX of the BNR MBR options is countered by the higher OPEX costs resulting in the technology selection having no impact on the NPV assessment outcome.

## 12.6 Multi-Criteria Analysis

A Multi Criteria Analysis (MCA) was undertaken of the options considered. Six criteria were used being:

Cost (NPV)





- Constructability, including quality, environmental and safety risks, timeframe for completion, likelihood of
  exceeding discharge licence conditions and extent of temporary works.
- Operability, including potential for increase in operating costs, ability to operate, WHS for operational staff, extent of autonomy and remote capability.
- Sustainability, including impact on environment, ability to reuse effluent and biosolids and ability to capture gas and resource recovery.
- Future Proofing, including achieving licence, increasing capacity and accommodating unexpected increases in flows or influent quality.
- Community Acceptance and Affordability, including impact on rates and QPRC financial position and QPRC reputation.

The criteria were weighted via a workshop together with QPRC's Director of Projects and Assets - Phil Hansen, Water and Sewerage Manager - Andre Pretorius, Principal Engineer (Water and Sewerage) - Peter Cox and Project Support Engineer - Simon Boulton. This resulted in the following weightings for the selected criteria provided in Table 12-2 below.

Criteria	Weighting
Cost	14%
Constructability	4%
Operability	15%
Sustainability	13%
Future Proofing	17%
Community Acceptance and Affordability	37%

## Table 12-2 MCA Criteria Weighting

The criteria were then scored by the participants of the workshop with results and ranking as shown in Table 12-3 below:

#### Table 12-3 MCA Results and Rank

Criteria	Options						
	Option 1A	Option 1B	Option 2A	Option 2B	Option 3A	Option 3B	
Cost	4.9	4.9	4.8	4.9	5.0	4.9	
Constructability	4.3	4.3	2.7	2.7	2.3	2.3	
Operability	4.3	4.0	3.3	3.0	3.3	3.0	
Sustainability	4.3	4.3	4.0	4.0	4.0	4.0	
Future Proofing	3.7	4.3	3.7	4.3	3.7	4.3	
Community Acceptance and Affordability	3.7	3.7	2.7	2.7	2.2	2.2	
Normalised Score	99	100	83	85	79	80	
Rank	2	1	4	3	6	5	

The MCA normalised scores indicate that Options 1A and 1B are difficult to separate and represent the preferred options. Options 2A and 2B similarly have close scores but are clearly separated in their ranking at 3rd and 4th





and Options 3A and 3B also have close scores and are 5th and 6th in their ranking. The sub options of A and B based on the process selection can be seen to have no impact on the selection of the upgrade approach.

The sensitivity of the MCA outcome was then tested for the following criteria weighting scenarios:

- All criteria equally weighted
- Each criterion in turn considered the most important with 50% weighting and all other criteria with 10% weighting each.

Irrespective of the scenario selected above, the Options 1A and 1B always ranked the highest indicating that the selection is not particularly sensitive to the weightings adopted for the various criteria.

## 12.7 Concluding Remarks

The assessment presented in Technical Memorandum TM004 concluded that the "Build New" strategy is the preferred option. Financially, the options cannot be separated with the key considerations being Community Acceptance, Operability, Sustainability and Constructability.





## 13 Risk Based Cost Estimate

## 13.1 Approach

A risk based project total cost estimate has been prepared for the Stage 1 upgraded STP, i.e. a 60,000 EP sewage treatment plant at the existing STP site. This is in line with the proposed upgrade option presented in this Masterplan. Further options analysis is required prior to development of future stages and as such these have not been costed here.

The mean estimated project value for the first stage development is \$108 million. The maximum estimated project budget cost is \$140 million. This value includes:

- Consulting services for
  - Project management
  - Planning and design (including site survey and geotechnical surveys)
  - Environmental studies
  - Construction superintendence
  - Construction administration
- QPRC staff inputs
- Capital works cost
- Stakeholder and regulatory engagement
- Reimbursable items for QPRC staff and Consultants.

The cost estimate does not include decommissioning and site rehabilitation costs for the existing STP facility or costs for connecting the Tralee development to the Jerrabomberra Trunk Sewer. The cost estimate also does not include operating costs or ancillary costs such as land purchase (as existing site is proposed to be maintained).

The estimate has been prepared with consideration for the likely outcome of costs but, due to the early nature and scope of this work, it is possible that the final costs may vary from this estimate. This is illustrated in Figure 13-1, which shows a risk based spread of the likely overall project cost estimate. It should be noted that a rigorous scope analysis has not been undertaken and budget estimates have been prepared on the scope known at this time.

The cost estimate has been based on assuming the concept design is a relatively complete reference design (75% design) and the detailed design is assumed to be about 70 to 80% of the concept design effort.

The project planning horizon is 50 years and the project timeframe for the initial upgrade (60,000 EP) is assumed to be six years. Additional costs would be incurred for delivery of future stages of the STP (or decentralised alternative sites) for meeting future demands of the Queanbeyan LGA.







## TOTAL ESTIMATED PROJECT BUDGET (Incl GST) ...



#### **Concluding observations** 13.2

Overall, the QPRC cost estimate is likely conservative, but (as noted in the estimate), given the project is probably five or more years from delivery, this conservative approach is appropriate. It is appropriate to proceed with the project on the basis of the QPRC derived project budget cost.





## 14 Stakeholders

Various engagement activities have been held with stakeholders from Federal, State (NSW and ACT) and Local Government, as well as QPRC business units.

The key stakeholder and regulatory agencies are listed in the Register provided at Appendix E.

The Project Management team holds the Register in full. The Register includes attendance at workshops and contributing comments. This will be a live document as the project progresses through the next phases, updated by the project management team.

## 14.1 Engagement

A preliminary briefing to regulators was held on 29 May 2014 that gave an overview of the project and the indicative timeframes for delivery.

A Masterplan briefing to regulators was held on 13 February 2015. This workshop provided an overview of the findings from the Masterplan and the proposed options to be taken through to concept design. The outcomes of this workshop have been incorporated into this Masterplan document.

The main items coming from the workshop included:

- Keen to investigate a regional / cross border arrangement
- Phosphorus discharge needs to be considered in light of the phosphorus budget for LBG
- Comfortable with the options proposed
- Need to consider recycled water
- Continue to liaise on Road Map options.

## 14.2 Community consultation

Community consultation for this project will be undertaken as part of QPRC's commitment to the Infrastructure Sustainability Rating Scheme and obtaining a certified "Excellent" rating for the new infrastructure.

QPRC subscribes to the foundations of public participation advocated by the International Association for Public Participation IAP<sup>2</sup>. QPRC will undertake decision making by actively seeking community participation in the options process. QPRC will actively be responsive the publics suggestions and concerns in finalising the preferred option.

It is hoped that through this process QPRC will develop infrastructure that is designed, optimise environmental, social and economic outcomes, which includes considering and consulting on the social / public aspects of the decision process.





## **15** Interim and transition infrastructure requirements

It is acknowledged that the planning, design and construction of a new STP will take time. In the meantime, the existing plant must be kept operational, meeting licence requirements. As such, a review of current operations was undertaken and options for interim operating improvements were investigated. These options are summarised here and the technical memoranda are presented in Appendix J.

## 15.1 Inlet screens

The existing screens were not effectively removing screenings and, due to age, prone to failure. A review of the current screens was undertaken and the following recommendations and actions were made.

- The existing functional mechanically-raked bar screen be replaced with either a step screen or spiral sieve screen. Both types are suited to retrofitting in existing channels. Irrespective of the relative capture rates for these different screen types, the screens will capture a significantly higher volume of screenings than the existing screen with 20 mm aperture
- QPRC to further consider the offer from VoR Environmental with respect to the option of immediate delivery of a reconditioned 3 mm aperture Meva step screen compared to a 6 mm CFC700 spiral sieve screen with a compactor but with a delivery time of up to 18 weeks
- The offer from VoR Environmental is for supply and delivery only. The costs for the full installation should be further investigated
- When the William Boby screen in the west channel is being used, install stopboards at the discharge into the disused Grit Chamber No. 1 so that the flow is directed to the Vortex Flow Grit Trap
- Hydraulic analysis to be undertaken to assess the benefits of the Installation of a weir plate on the overflow from the main screen channel to reduce the volume of wet weather overflow to the manually raked bypass screen
- QPRC approach the ACT Government to allow the screenings to be disposed of at the Mugga Lane landfill

As a result of an in parallel to this review QPRC undertook a refurbishment of the existing screen. This refurbished screen was reinstalled in the channel with reduced aperture (12 mm) and is working effectively.

## 15.2 Final clarifiers

Scum is accumulating on the surface of the final clarifiers, which leads to the operators having to regularly hose the surface of the clarifiers to remove and break up the surface scum, in an attempt to control the build-up of scum. The operators have also removed a short section of the scum baffle in an attempt to alleviate this problem. It is reported that the depth of scum on the surface of the clarifiers exceeds the height of the outer scum baffle at times.

The existing scum surface skimmer/scraper and associated scum beach and chute are currently not operational and are in a condition of disrepair, such that they are ineffective in removing scum from the final clarifiers. Scum that may be removed from the clarifiers through the surface skimmer arrangement, gravity flows to the return activated sludge (RAS) pump station/s and is returned to the bioreactors with the RAS.

The scum overflowing the clarifiers with the effluent flow is arrested on the surface of a small inlet lagoon before the flow passes into the main tertiary lagoons.

In order to control the surface scum accumulation on the final clarifiers, the following options have been considered:

• Encourage scum to flow with the clarifier effluent to the Tertiary Lagoons





- Remove scum from the clarifiers by re-instating the existing final clarifier scum mechanisms and peripheral scum baffles, to effectively remove the surface scum from each of the clarifier surfaces
- Reduce potential for scum growth by operating at lower sludge retention time in the biological process.

## 15.3 Sludge Lagoons

Currently the sludge from the activated sludge process is wasted to either of two lagoons, where it is stored and stabilised prior to drying on the site's sludge drying beds. Only one of the sludge lagoons is fed over a period (approximately 6 to 12 months). When that lagoon is filled, then the sludge is directed to the other (empty) lagoon. The filled lagoon is then pumped out to the sludge drying beds, so that it is emptied prior to the other lagoon completely filling. When the sludge has sufficiently dried on the drying beds, it is removed and stockpiled on site.

The stockpile area is at capacity and an alternative needs to be found in the short-term. In addition, the sludge drying beds are at capacity, so that the sludge lagoons are filled before the sludge on the drying beds is sufficiently dried.

## 15.4 Timing

These interim measures should be undertaken as soon as possible.





## 16 Approvals

QPRC operates a STP on land bordering the Molonglo River within the ACT. The collection system for this STP is located in NSW and the discharge is to the Molonglo River, which flows to Lake Burley Griffin (LBG). The National Capital Authority, a Federal Government department, manages LBG. This regulatory inter-relationship makes the approvals process complex.

Infrastructure is required to ensure the capacity of the STP can meet the demands of the Queanbeyan community and reliably protect the environment and public health 50 years into the future and planning for this is underway.

The following defines the land on which the sewage treatment plant currently operates:

Block 27 Jerrabomberra (Rural Proposed):

• Block 2087 Jerrabomberra (Rural Registered).

The blocks (herein referred to as 'the site') are currently leased from the ACT Government by QPRC. It is understood that there are less than 20 years remaining on the existing lease title (lease expires 1 April 2023).

The boundaries of block 2087 and 27 Jerrabomberra are slightly different and clarification of the site boundaries should be sought prior to completing concept designs and applying for statutory approvals.

The following sections briefly identify the anticipated regulatory approval process for the development of a new sewage treatment facility within the current site boundaries.

A Regulatory Approvals Roadmap is provided in Appendix C. This would be updated during the project as required.

## 16.1 Planning

## 16.1.1 Development Application

The site is located in the ACT on Territory Land and is therefore subject to the requirements of the ACT *Territory Plan 2008.* The site is zoned as TSZ2: Services and NUZ4: River Corridor land uses under the Territory Plan.

The proposed activity requires an environment impact statement (EIS) under Schedule 4 of the ACT *Planning and* Development *Act 2007* (P&D Act) <sup>4</sup>.

ACT Health (together with the NCA) regulates discharges to Lake Burley Griffin. The Minister responsible for the ACT *Public Health Act 1997* has the ability to declare the proposal impact applicable and therefore requiring an EIS to be undertaken.

(ii) 750kL; or

<sup>&</sup>lt;sup>4</sup> proposal for construction of a wastewater treatment plant (including a plant for the treatment of sewage or other effluent) that— (a) will be less than 1km from the boundary of a residential block or unit in a residential or commercial zone; or

<sup>(</sup>b) will be able to treat each day more than-

<sup>(</sup>i) 2 500 people equivalent capacity; or

<sup>(</sup>c) will have capacity to store more than 1kt of sewage, sludge or effluent; or

<sup>(</sup>d) will incinerate sewage or sewage products; or

<sup>(</sup>e) will have a capacity to treat more than 100ML of wastewater (excluding stormwater) each year; but f) is not—

<sup>(</sup>i) a plant for the treatment of stormwater; or

<sup>(</sup>ii) a small-scale wastewater treatment plant (including a plant for the treatment of sewage or other effluent but not including a small-scale plant prescribed by regulation); or

<sup>(</sup>iii) a residential on-site wastewater treatment system (including a septic tank)





It is unlikely that this will occur given that an EIS is already required and that the proposal will improve the quality of the inputs into the Molonglo River and other receptors. Nevertheless, consultation with ACT Health would likely be required as part of the EIS preparation.

The construction of a "sewage treatment facility" is not a prohibited activity in the zones (TSZ2: Services and NUZ4: River Corridor).

The Development Application (DA) would likely be assessed under the Impact Track. A completed EIS is required to be submitted with a Development Application submitted under the Impact Track. This applies to the whole site zoned TSZ2: Services and NUZ4: River Corridor (small areas bordering the Molonglo River).

Any development undertaken on the site must meet the requirements of the Transport and Services Development Code and the Non-Urban Zones Development Code.

At this stage, there does not appear to be anything to differentiate potential developable areas of the site in relation to the DA path. All areas are likely to require assessment under the Impact Track.

If the existing STP was to be refurbished, there *may* be scope for the proposal to be assessed under the Merit Track, but this would require further investigation.

Demolition/decommissioning of the existing infrastructure *may* be able to be assessed under Merit Track, as demolition is listed as a permissible activity in the Services Zone Development Table. These activities are however likely to be included in any EIS undertaken for the proposal. Inclusion of these activities in the EIS would likely be the most efficient approval path.

## 16.1.2 National Capital Plan

Consultation with the NCA and compliance with the provisions of the Federal Government's *National Capital Plan* would likely be required. The NCA (together with ACT Health) regulate the discharge to Lake Burley Griffin. Specifically the requirements relating to Urban Areas, Broadacre Zones and Lake Burley Griffin, Hills Ridges and Buffers, River Corridors and Mountains and Bushland would likely need to be considered.

A Works Approval or Development Control Plan is unlikely to be required as the site is not located near any Designated Areas.

## 16.2 Environmental Approvals

## 16.2.1 Environmental Impact Assessment (EIA)

EIA is used to assess the impact of a project on the environment. Under ACT legislation, an EIS would be prepared as required for the STP upgrade DA (see Section 16.1.1 above) under the *P&D Act*. This would include various specialist studies that would be identified in a Scoping Document, which outlines what must be addressed in the EIS. The Scoping Document is prepared by the EPD.

In order to apply for a Scoping Document, a Preliminary Risk Assessment (PRA) must be completed in accordance with AS/NZS 14004:2004 Environmental Management Systems and AS/NZS ISO 13000:2009 Risk Management. The PRA must accompany the request for a Scoping Document.

The quality of the information provided with the Scoping Document application will determine the extent of work required to complete the EIS.

It is important that the application is not made until there is sufficient information to clearly understand the nature of the development and its potential impacts.

Similarly, if works are proposed in NSW (such as for the collection network), environmental approvals consideration would be required for this as well. It is possible that, depending on the scale of the works, QPRC could be the determining authority.





Continued engagement with EPD, ACT Government Stakeholders, NSW EPA and the NCA will be required throughout the preparation of the EIS.

## 16.2.2 Preliminary Environmental Assessment

Currently, there is not enough information known about the issues and constraints on the site and therefore the impacts likely to occur from the proposal to inform the Scoping Document. A Preliminary Environmental Assessment could be undertaken in the early Concept Design stages to enable sufficient information to be gathered for both the design and the Scoping Document application.

## 16.2.3 Environmental authorisation

The proposal is also classified as a *Class A* activity under the ACT *Environment Protection Act 1997* and will therefore require an Environmental Authorisation for the operation of the site. QPRC already has an Environmental Authorisation for the existing plant that is reviewed on an annual basis. The current Environmental Authorisation states "1.1.5 The Authorisation holder shall seek the approval in writing of the EPA to install, construct or modify any equipment or works in or on the premises which would impact on the plant's capacity to achieve Authorisation conditions."

It should be noted that the current Environment Authorisation is for Block 2087 Oaks Estate (now known as Block 2087 Jerrabomberra). Clarification of the site should be made in the Authorisation, including the applicability of the approval to Block 27 Jerrabomberra.

## 16.2.4 Environment Protection Agreement

An Environment Protection Agreement may be required for *Class B* activities (under the ACT *Environment Protection Act 1997*) carried out during construction on the site. This would be confirmed once further information regarding the design and construction of the proposed sewage treatment plant is known.

#### 16.2.5 Waterway works licence

Works undertaken within the Molonglo River Corridor would likely require a Waterway Works License (ACT government). Further detail regarding the proposed design of the sewage treatment plant is required to determine the need for this approval.

#### 16.2.6 River discharge licence

A licence allowing treated wastewater to be discharged to the Molonglo River would likely be required. QPRC has an existing licence with the ACT that will need to be confirmed and updated during the project.

#### 16.2.7 Contaminated land management

As part of the EIS, a contamination assessment would likely be needed to determine the contamination status of the site and remedial actions that might be required.

Development of the site would be subject to the ACT *Contaminated Sites Environmental Protection Policy 2009* (EPP). It is likely the site is listed on the ACT Contaminated Sites Register; given sewage treatment plants are recognised in the EPP as a potential source of contaminants.

#### 16.2.8 Matters of National Environmental significance

As part of the EIS, an assessment under the Commonwealth *Environmental Protection and Biodiversity Conservation Act 1999* (EPBC Act) would likely be required to determine whether the proposal would have a significant impact on Matters of National Environmental Significance.

A Bilateral EIS process can potentially apply to proposals that require both an Environmental Impact Statement (EIS) under the ACT *P&D Act* and also approval from the Department of the Environment under the *EPBC Act*. The Australian Government has accredited the ACT's EIS process through a bilateral agreement as meeting the environmental assessment requirements of the EPBC Act.





If an EPBC Act referral is submitted to the Department of the Environment and if the proposed action is determined to be a controlled action under the EPBC Act and requires an EIS under the ACT *P&D Act*, the ACT Government may invoke the bilateral agreement. If the bilateral agreement applies the subsequent scoping document and EIS assessment report will be prepared by the ACT with input from the Australian Government.

### 16.2.9 Waste management

The management of waste from the proposed development, including waste generated from construction, demolition of existing infrastructure and waste products from the operation of the site must be considered.

Early consultation with ACT NOWaste and the ACT EPA regarding waste management would be required, particularly given the current shortage of landfill space in the ACT.

It is understood that wastewater and sludge are currently managed on site. It is also understood that solids management is unlikely to be undertaken on site in the new STP design.

Additional approvals would likely need to be sought from EPD, QPRC, ACT NOWaste, ACT EPA and NSW EPA to allow management of biosolids to occur at the proposed end point. The current Environmental Authorisation states "3.2 Reuse of sewage sludge in the ACT should be in accordance with the National Water Quality Management Strategy Draft Guidelines for Sewage Systems Sludge (Biodsolids) Management 1998."

The concept design should be progressed to demonstrate how sludge would be managed (i.e. level of dewatering and treatment) such that biosolids could be able to be moved and processed (reused or disposed of) appropriately off-site. The EIS can likely be submitted prior to identifying the final end-point of the biosolids; however this will require further confirmation and consultation with the EPD and the relevant stakeholders.

In addition, approvals would likely be required to allow transportation of waste outside of the ACT.

## 16.3 Infrastructure approvals

Section 60 of the NSW Local Government Act (1993) requires DPI Water to approve:

A council must not, except in accordance with the approval of the Minister for Primary Industries, do any of the following:

- a. As to works of water supply-construct or extend a dam for the impounding or diversion of water for public use or any associated works
- b. As to water treatment works-construct or extend any such works
- c. As to sewage-provide for sewage from its area to be discharged, treated or supplied to any person
- d. As to flood retarding basins prescribed by the regulations-construct or extend any such basins.

DPI Water provide approval following a 5 Step process for a detailed design and construction procurement, as indicated in Figure 16-1. QPRC are required to involve DPI Water at each Step and seek their consultation and formal endorsement. Essentially this means that the following documents are submitted and approved:

- Masterplan and options report
- Concept design report
- Detailed design report.

(http://www.water.nsw.gov.au/Urban-water/Country-Towns-Program/Best-practice-management/Regulations-for-water/Water-and-sewage-treatment-works/Construction-of-a-detailed-design/default.aspx).

The NSW Government's Best-Practice Management of Water Supply and Sewerage Framework require local water utilities to prepare and implement a sound 30-year Integrated Water Cycle Management (IWCM) Strategy, which includes a Financial Plan. The IWCM, which must be submitted to and approved by DPI Water, is closely linked to the Section 60 approvals process. A 30-year IWCM Strategy addresses the complex linkages between elements





of the urban water cycle (water supply, sewage and stormwater) and community expectations. This is done within the urban area and between the urban area and its water related physical and legislative operating environment. This multi-level, transparent and systematic approach encourages cost-effective integration of these urban water systems in consultation with the local community.

(http://www.water.nsw.gov.au/Urban-water/Country-towns-program/Best-practice-management/Integrated-Water-Cycle-Management/default.aspx)

This requirement is likely to be associated with any funding support requested by QPRC.




Step	Local water utility	NSW Office of Water
1 Initial consultation	Write to the Office of Water about the problem identified and the proposal to investigate the need for water or sewage treatment works.	<ul> <li>Send an acknowledgement letter to the utility.</li> <li>Provide advice to the utility about the options study required for the proposed works.</li> <li>Meet with the utility for discussion if needed</li> </ul>

2	Options study	<ul> <li>Provide a draft options study report to the Office of Water.</li> <li>Arrange revision and finalisation of the report, incorporating comments from the Office of Water</li> </ul>	<ul> <li>Review the draft options report.</li> <li>Provide comments to the utility.</li> <li>Meet with the utility to discuss the comments if needed.</li> </ul>
		incorporating comments from the Office of Water.	<ul> <li>the comments if needed.</li> <li>Endorse the final report.</li> </ul>

3	Concept design	<ul> <li>Provide a draft concept design report to the Office of Water.</li> <li>Arrange revision and finalisation of the report, incorporating comments from the Office of Water</li> </ul>	<ul> <li>Review the draft concept design report.</li> <li>Provide comments to the utility.</li> <li>Meet with the utility to discuss the comments if needed.</li> </ul>
		from the Office of Water.	<ul> <li>Endorse the final report.</li> </ul>

4 De	etailed design	•	Provide a draft detailed design report to the Office of Water. Address all issues and design changes raised by the Office of Water.	<ul> <li>Assess key aspects of the detailed design to ensure that it has adequately addressed all issues and meets the requirements of a robust, safe and soundly based and cost- effective solution.</li> </ul>
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	<ul> <li>Provide comments to the utility and request essential changes. Meet with the utility if needed.</li> </ul>
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5	Section 60 approval	<ul> <li>Provide the amended detailed design report to the Office of Water</li> </ul>	•	Review the design changes made by the utility.
		and office of Water.	•	issue Section of approval.







## 16.4 IWCM

The NSW Government has promoted continuing performance improvement across local water utilities, with the aim of improving the quality and efficiency of services to the NSW community. Performance monitoring and reporting has been aligned with the National Water Initiative, which operates at a Federal level. The first benchmark performance report was released for the 2005/06 financial year.

Since that time, the performance monitoring framework and associated reporting approaches and mechanisms has continually improved, most recently with the changes to the Integrated Water Cycle Management (IWCM) component, to which this project will contribute.

The NSW Government, via the Office of Water, contends that local water utilities which follow the Best Practice Management Framework will demonstrate and achieve more effective and sustainable water supply and sewerage services. It follows that adoption and implementation of such best practice frameworks at a local water utility level, through mechanisms such as IWCM, will provide for this.

The Framework is a key driver for planning reform and continuous performance improvement. The 19 requirements of the Framework are prescribed in the Best Practice Management of Water Supply and Sewerage Guidelines, which sit across 6 key elements including:

- 1. Integrated Water Cycle Management
- 2. Strategic business planning
- 3. Regulation and pricing of water supply, sewerage and trade waste:
  - Pricing
  - Developer charges
  - Liquid trade waste
- 4. Water conservation
- 5. Drought management
- 6. Performance monitoring.

In its purest form, the Framework allows for public accountability of the local water utility to the communities it serves, and provides verification of agreed service delivery standards. In addition, the framework supports the intent of the Water Management Act 2000 to protect human health and the environment. The framework support comes from using triple bottom line accounting to achieve a balance between financial, social and environmental outcomes.

Going forward, the Best Practice Management Framework will likely underpin the current Fit for the Future reform program, which NSW local councils must comply with. The NSW Government suggests that regional Joint Organisations be established to provide a platform for local council collaboration to achieve regional outcomes and maximise efficiencies. Joint organisations will likely be established along consistent regional boundaries, to reduce duplication and facilitate collaboration and this may impact QPRC. Financial support will depend on Councils demonstrating being 'fit for the future' and able to deliver capital infrastructure, which can be successfully (sustainably) operated over the long term.

DPI Water has advised QPRC that it should prepare and implement an IWCM for the whole LGA.

http://www.water.nsw.gov.au/Urban-water/Country-towns-program/Best-practice-management/Integrated-Water-Cycle-Management/default.aspx





## 17 Basis of design outcome

The observations made throughout this masterplan are summarised in Table 17-1 and will form the basis of design for the STP, informing the Concept Design Stage.

Table 17-1	Basis of design
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Masterplan Element	Design Basis Outcome
Best for region Solution	Queanbeyan's location on the border of NSW and the ACT puts it in a unique position. The STP is located in the ACT on leased land and ACT Environment and Planning Directorate (EPD) (which includes the Environment Protection and Water Regulation Division), ACT Health and the National Capital Authority (NCA) regulate various aspects of the STP operations. Potential regional opportunities for wastewater management are subject to ongoing discussion with the ACT Government and Icon Water.
Future Growth	Growth is expected to occur in the middle portion of the LGA within the 10 – 25 year horizon. The southern third of the LGA is then expected to grow during the 25 – 50 year horizon. Provision for the first stage of the Queanbeyan STP Upgrade should be for an EP of 60,000. This provides for the 10 to 15 years' growth projection. It should be noted that the projections within this Masterplan do not make allowance for any ACT contribution to sewage flows, though depending on timing of actual increases, some flow may be able to be accommodated. The EP calculator was based on average water data for Queanbeyan LGA averaged over 2009- 14.
Existing Sewerage Infrastructure	The existing Queanbeyan STP condition currently presents a risk to QPRC with numerous suggestions for both immediate and short-term improvement. Beyond operability and WHS issues, there will be a stronger focus on water quality and environmental discharges. Tighter discharge criteria are likely to be imposed in the future when licence conditions are renegotiated.
Future Sewerage Infrastructure	<ul> <li>The South Jerrabomberra sewer trunk will need to be upgraded to meet future capacity: <ul> <li>Consider augmentation of the Jerrabomberra Trunk Sewer between manholes W8 and the inlet channel of the STP</li> <li>Any further augmentation should be delayed until a final service strategy is decided for future development to the south of Queanbeyan</li> <li>A survey and sewer gauging program should be implemented for the whole length of the trunk sewer (manhole W78 to the STP inlet channel) to enable a more detailed analysis of the sewer</li> </ul> </li> <li>Continue discussions with Icon Water around cross-border arrangements and a regional approach to sewage management.</li> <li>A septic tank receival station should be included in the new plant.</li> </ul>
Environmental Constraints	<ul> <li>The following should be considered when determining the location for future STP(s):</li> <li>Avoid heritage listed sites, scenic protection areas, and quarry buffer zone</li> <li>Construction within the ANEF affected areas could be considered if appropriate as aircraft noise is unlikely to be an impact on STP operations</li> <li>Avoid infrastructure within the Q100 flood level without proper flood protection or mitigation measures in place</li> <li>Avoid bushfire prone areas or provide adequate protections, appropriate to STP operations</li> <li>Consider and incorporate mitigation of environmental issues on existing site as part of concept design.</li> </ul>





Masterplan Element	Design Basis Outcome						
Water Quality	Adopt the following effluent discharge criteria and 100% river discharge as the basis of design outcome.						
	Parameter	Units	Performance	Statistic	Proposed Licence Limit (100%ile)		
	Total Nitrogen	mg/L	10 5	90%ile 50%ile	10		
	Total Phosphorus	mg/L	0.15 0.1	90%ile 50%ile	0.2		
	Faecal coliforms	cfu/100mL	30 200	Median 90%ile	60		
	BOD	mg/L	10 5	90%ile 50%ile	10		
	Suspended Solids	mg/L	10 5	90%ile 50%ile	10		
Sustainability	<ul> <li>Set sustainability targets with the goal of obtaining IS design and as-built ratings of Excellent with a score in the range of 65 – 75% or better.</li> <li>Undertake a recycled water study to determine the viability of reuse in the future which addresses impacts on:</li> <li>1. Discharge to the Molonglo River</li> <li>2. Molonglo River yield and downstream environmental flows</li> <li>Aquatic species along the Molonglo River</li> </ul>						
Solids Management	<ul> <li>The solid management solution comparison showed that the most beneficial options were:</li> <li>Reuse for land reclamation</li> <li>Production of fertiliser for animal crops</li> <li>Production of fertiliser for human crops</li> <li>Use for horticulture and landscaping.</li> <li>The concept design phase should develop and consider these options further, however if other feasible options become apparent then these may also be considered.</li> </ul>						
Treatment	Treatment Step	Preliminary	Option (to be co	nfirmed at Conce	pt Design stage)		
lechnologies	Preliminary	Inlet works s the seconda	Inlet works screenings and grit removal to be determined by choice of the secondary treatment process.				
	Primary	Equalisation tanks or Primary settling and possible use of mechanical belt sieve.					
	Secondary (one of)	BNR Bio-Rea Membrane Conventio – Si La – Pa	actor plus one of e Bioreactor (MBF onal Activated Slue equencing Batch agoons (SBR/IDA asveer/Oxidation	R) dge (CAS), e.g. Reactor/ Intermitte L) ditch	ently Decanted Aerated		
	Tertiary (one of)	<ul><li>Tertiary Fi</li><li>Refurbishi</li></ul>	iltration ing secondary cla	rifiers			
	Disinfection	UV Chlorine (if re	equired for regulat	ory purposes)			





Masterplan Element	Design Basis Outcom	ie	
	Solids	Grit and Screenings - Landfill	
	Biosolids (one of or a combination of)	<ul> <li>Land reclamation</li> <li>Animal crop production</li> <li>Landscaping – Composting</li> <li>Other options may be considered if they can be shown to be feasible through a regional approach.</li> </ul>	
Upgrade Approach	A Multi Criteria Assessment found that a "Build New" upgrade approach was preferred taking into account whole of life cost, constructability, operability, sustainability, future proofing and community acceptance and affordability. All options including build new, refurbishment and reuse options provided a whole of life NPV around \$100 M. The total project cost estimate prepared by QPRC using @risk modelling showed a mean estimated project value of \$108 M. The assessment of plausible refurbished and reused assets showed no significant capital investment saving compared to the build new option cost estimates. All estimates are preliminary and based on a range of caveats. There is no discernible significant difference within the sensitivity of the cost analysis at a Masterplan level. The selection of treatment technology (BNR – CAS v BNR – MBR) was not significant to the outcome.		
Approvals	ACT Approvals Under Schedule 4 of th upgrade to the STP wo A Development Applica Impact Track. The corr submitted under the Im NUZ4: River Corridor ( <i>NSW Approvals</i> NSW approvals will be system). The NSW leg consideration (such as approving authority for NSW would be require NSW Office of Water is <i>Government Act (1993)</i> <i>Federal Approvals</i> Any works approval so <i>Conservation Act 1993</i>	he ACT <i>Planning and Development Act 2007</i> (P&D Act) the proposed build require an environment impact statement (EIS). ation (DA) would also be required and would likely be assessed under the impleted EIS is required to be submitted with the Development Application inpact Track. This applies to the whole site zoned TSZ2: Services and small areas bordering the Molonglo River). required for any works within NSW (such as the sewerage collection gislation would similarly require Development Approval and environmental contaminated lands and endangered species). It is possible that the this work could be QPRC. Further detail of the scope of any works in d to determine this. s required to approve the STP upgrade under Section 60 of the <i>Local</i> and the state of the state of the state of the state of the state and state of the state and the state of the state	
	General Comments In 2015 the interim AC by the ACT Environme Stakeholders. The func- management approach Griffin. Continued engagemen be required regarding L preparation of the EIS. Local Councils are required outlined by the NSW O	T and Region Catchment Management Coordination Group was formed nt Minister. This group includes EPD, and other ACT Government ction of this committee is to implement an integrated catchment in the ACT and Region, including improving water quality in Lake Burley t with EPD, ACT Government Stakeholders, NSW EPA and the NCA will ake improvement through an agreed approach and throughout the A framework for a joint approach is agreed. uired to produce an Integrated Water Cycle Management (IWCM) plan ffice of Water.	





## 18 References

MWH (2008), Queanbeyan Sewage Treatment Plant Future Needs Study Final Report. HWA (2011), Queanbeyan Sewage Treatment Plant Upgrade Options Assessment Summary Report.